

(2) (1)

PATENT ABSTRACTS OF JAPAN

(11)Publication number : 2001-086715

(43)Date of publication of application : 30.03.2001

(51)Int.Cl.

H02K 19/22

(21)Application number : 11-264130

(71)Applicant : MITSUBISHI ELECTRIC CORP

(22)Date of filing : 17.09.1999

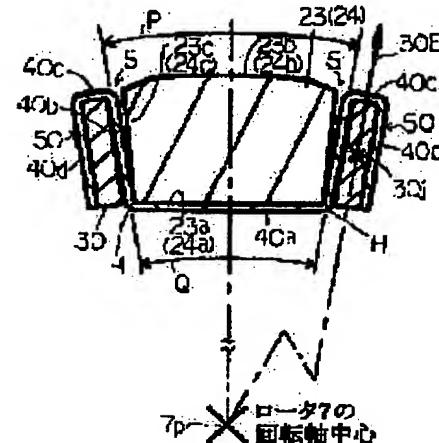
(72)Inventor : TONO KYOKO
ASAOKA YOSHITO
TSURUHARA KENJI
OHASHI ATSUSHI

(54) ROTOR STRUCTURE

(57)Abstract:

PROBLEM TO BE SOLVED: To reduce centrifugal force applied during rotation of a rotor by providing a pole core having claw poles projecting to mesh each other, and a reinforcing body included such that the outer circumferential surface of a magnet for reducing flux leakage from the side face of adjacent claw pole enlarges mutually.

SOLUTION: A magnet 30 is provided on side faces 23c, 24c of a claw pole 23, 24, while inclining in a direction of enlarging from the center line thereof passing through the center of rotation 7p of a rotor 7 toward the outer circumferential surface 23b, 24b side and thereby no holding part is required. It is cantilevered by a reinforcing body 40 using adhesives. A centrifugal force 30E, being applied to the center of gravity 30j of the magnet 30 during rotation of the rotor 7, is absorbed by the reinforcing body 40 in the form of a moment for turning the magnet 30 and a part of the reinforcing body 40 for holding the magnet 30. Since a side face magnet body 50 turns such that the outside diameter side thereof approaches the side 23c, 24c of the claw pole, the stress becomes less than an allowable range.



LEGAL STATUS

[Date of request for examination] 12.02.2002

[Date of sending the examiner's decision of rejection]

[Kind of final disposal of application other than the examiner's decision of rejection or application converted registration]

[Date of final disposal for application]

[Patent number] 3532130

[Date of registration] 12.03.2004

[Number of appeal against examiner's decision
of rejection]

[Date of requesting appeal against examiner's
decision of rejection]

[Date of extinction of right]

Copyright (C); 1998,2003 Japan Patent Office

(19)日本国特許庁 (JP)

(12) 公開特許公報 (A)

(11)特許出願公開番号

特開2001-86715

(P2001-86715A)

(43)公開日 平成13年3月30日 (2001.3.30)

(51)Int.Cl.'

H 02 K 19/22

識別記号

F I

H 02 K 19/22

テ-マコト(参考)

5 H 6 1 9

審査請求 未請求 請求項の数20 O.L (全 15 頁)

(21)出願番号 特願平11-264130

(22)出願日 平成11年9月17日 (1999.9.17)

(71)出願人 000006013

三菱電機株式会社

東京都千代田区丸の内二丁目2番3号

(72)発明者 東野 恭子

東京都千代田区丸の内二丁目2番3号 三菱電機株式会社内

(72)発明者 浅尾 淑人

東京都千代田区丸の内二丁目2番3号 三菱電機株式会社内

(74)代理人 100080296

弁理士 宮園 純一

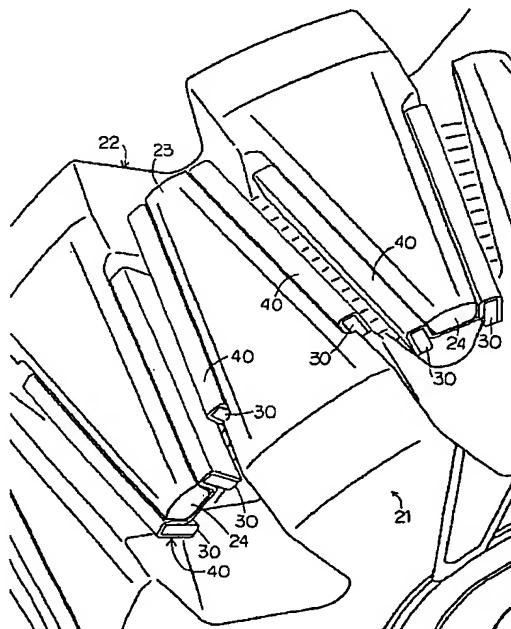
最終頁に統く

(54)【発明の名称】 ロータ構造

(57)【要約】

【課題】 爪状磁極同志の磁束漏洩を防止する磁石に加わる遠心力を低減する。

【解決手段】 爪状磁極23, 24の両側面23c, 24cに配設され、爪状磁極23, 24同志の磁束漏洩を低減する磁石30と、この磁石30を外周側が互いに広がるように傾斜する如く支持する補強体40とを備えた。



〔特許請求の範囲〕

〔請求項1〕 磁束を発生するロータコイルと、このロータコイルを覆って設けられ、交互に噛み合うように突出される爪状磁極をそれぞれ有する第1のポールコア体及び第2のポールコア体から構成されたポールコアと、上記爪状磁極の両側面側に配設され、隣り合う爪状磁極の側面同志の磁束の漏洩を低減する磁石と、この磁石を外周側が互いに広がるように傾斜する如く支持する補強体とを備えたことを特徴とするロータ構造。

〔請求項2〕 上記補強体は、爪状磁極の内周面に沿う内周部と、この内周部の両端から爪状磁極の側面へ折曲された折曲部と、この折曲部から折曲された磁石の外周面を押さえ付ける押さえ付け部と、押さえ付け部から磁石の外周面へ折返された折り返し部とより成り、補強体の内周側に上記磁石を支持したことを特徴とする請求項1に記載のロータ構造。

〔請求項3〕 上記補強体は、爪状磁極の内周面と磁石の内周面に沿う内周部と、この内周部の両端から磁石の側面へ折曲された折曲部と、この折曲部から爪状磁極に突出して爪状磁極の外周面を押さえ付ける押さえ付け部とより成り、補強体の外周側に上記磁石を支持したこととを特徴とする請求項1に記載のロータ構造。

〔請求項4〕 上記磁石と補強体の磁石を支持した部分とにより側面磁石体を構成して、この側面磁石体と上記爪状磁極の側面との間に間隙を設け、上記磁石に遠心力が加わったときに、側面磁石体が爪状磁極側に上記間隙を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収することとを特徴とする請求項2又は請求項3に記載のロータ構造。

〔請求項5〕 上記側面磁石体の回動中心は、ロータの回転軸中心と磁石の重心とを結ぶ線よりも爪状磁極側に位置され、上記側面磁石体の回動は、爪状磁極の側面に当接することで係止されることとを特徴とする請求項4に記載のロータ構造。

〔請求項6〕 上記押さえ付け部と折り返し部とで磁石を支持して磁石とともに側面磁石体を構成し、この側面磁石体と上記爪状磁極の側面との間に間隙を設け、かつ隣り合う側面磁石体の相互間に間隙を設け、上記磁石に遠心力が加わったときに、側面磁石体が隣り合う側面磁石体側に上記側面磁石体相互間の間隙を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収し、上記側面磁石体の回動は、隣り合う保持部同志が当接して互いに係止し合うことを特徴とする請求項2に記載のロータ構造。

〔請求項7〕 上記側面磁石体と上記爪状磁極の側面との間の間隙は、上記側面磁石体の回動が係止されて補強体の変形量が最大になってから上記磁石に遠心力が加わらなくなつたときに、変形した補強体が元の形状に戻るよう、離間されたことを特徴とする請求項4又は請求項6に記載のロータ構造。

〔請求項8〕 上記側面磁石体と上記爪状磁極の側面との間の間隙は、上記側面磁石体の回動が係止されて補強体の変形量が最大になったときに補強体に加わる応力が、少なくとも許容応力以下となるように、離間されたことを特徴とする請求項4又は請求項6に記載のロータ構造。

〔請求項9〕 上記側面磁石体と上記爪状磁極の側面との間の間隙には、弾性体を介在させたことを特徴とする請求項4又は請求項6に記載のロータ構造。

〔請求項10〕 上記爪状磁極から補強体が内周側へ抜けることを防止する抜け止め構造を有することとを特徴とする請求項1ないし請求項6のいずれかに記載のロータ構造。

〔請求項11〕 上記爪状磁極から補強体が先端側へ抜けることを防止する抜け止め構造を有することとを特徴とする請求項1ないし請求項6のいずれかに記載のロータ構造。

〔請求項12〕 上記爪状磁極から補強体が内周側、先端側へ抜けることを防止する抜け止め構造を有することとを特徴とする請求項1ないし請求項6のいずれかに記載のロータ構造。

〔請求項13〕 上記抜け止め構造は、上記補強体より突出して爪状磁極の外周面に当接する当接部であることを特徴とする請求項10ないし請求項12のいずれかに記載のロータ構造。

〔請求項14〕 上記抜け止め構造として、上記補強体を内周側から爪状磁極に押さえ付ける押さえ付け部材を用いたことを特徴とする請求項10ないし請求項12のいずれかに記載のロータ構造。

〔請求項15〕 上記押さえ付け部材は、円筒状の外周面を有し、この外周面には補強体が組付けられた爪状磁極がはまる溝が形成され、爪状磁極の外周面と共にロータの外周面に円筒状の曲面を構成することとを特徴とする請求項14に記載のロータ構造。

〔請求項16〕 上記爪状磁極の側面は、内周側よりも外周側に広がる向きに傾いた傾斜角度を有することとを特徴とする請求項1ないし請求項15のいずれかに記載のロータ構造。

〔請求項17〕 上記磁石の重心は、爪状磁極の根元側に片寄って配置されることとを特徴とする請求項1ないし請求項16のいずれかに記載のロータ構造。

〔請求項18〕 上記補強体は、金属製であることを特徴とする請求項1ないし請求項16のいずれかに記載のロータ構造。

〔請求項19〕 上記補強体は、爪状磁極に溶接で固定されることとを特徴とする請求項18に記載のロータ構造。

〔請求項20〕 上記補強体は、磁石が補強体の先端側、根元側へ抜けることを防止する抜け止め構造を有することとを特徴とする請求項1ないし請求項16のいずれかに記載のロータ構造。

かに記載のロータ構造。

【発明の詳細な説明】

【0001】

【発明の属する技術分野】本発明は、交流発電機あるいは電動機のロータ構造、特に爪状磁極同志の磁束漏洩を防止する磁石の取り付け構造に関するものである。

【0002】

【従来の技術】図17は従来の交流発電機あるいは電動機のロータ構造を示す側断面図、図18はこのロータの構成を示す斜視図であり、図20はこのロータを部品単位で分解した側面図である。図17に示す如く、この発電機は、アルミニウム製のフロントブラケット1及びリヤブラケット2から構成されたケース3と、このケース3内に設けられ、一端部にブーリ4が固定されたシャフト6と、このシャフト6に固定されたランドル型のロータ7と、ロータ7の両端面に固定されたファン5と、ケース3内の内壁面に固定されたステータ8と、シャフト6の他端部に固定されロータ7に電流を供給するスリップリング9と、スリップリング9に搭動する一対のブラシ10と、このブラシ10を収納したブラシホールダ11と、ステータ8に電気的に接続されステータ8で生じた交流を直流に整流する整流器12と、ブラシホールダ11に嵌着されたヒートシンク19と、このヒートシンク19に接着されステータ8で生じた交流電圧の大きさを調整するレギュレータ20とを備えている。

【0003】ロータ7は、電流を流して磁束を発生する円筒状のロータコイル13と、このロータコイル13を覆って設けられ、その磁束によって磁極が形成されるポールコア14とを備えている。ステータ8は、ステータコア15と、このステータコア15に巻回され、ロータ7の回転に伴ってロータコイル13からの磁束の変化で交流が生じるステータコイル16とを備えている。ポールコア14は、一対の交互に噛み合った第一のポールコア体21及び第二のポールコア体22から構成されている。ポールコア体21及びポールコア体22は通常鉄製であり、ロータコイル13が巻装される円筒部21e、22eと、この円筒部21e、22eが突設された円盤状の基部21k、22kより成る。基部21k、22kの外縁には、ロータコイル13の外周とステータ8の内周との間に位置に、相互に噛み合う爪状磁極23、24をそれぞれ複数有している。上記爪状磁極23、24は、基部21k、22k側の厚み及び幅が大きく、先端側にいくに従って厚み及び幅が細くなる形状である。爪状磁極23、24の内周面23a、24aは、先端にいくにつれ厚みが薄くなり、外周面23b、24bは、ステータ8の内周面に沿った弧状である。爪状磁極23、24は、ロータ7の周方向に対して台形状の2つの側面23c、24cを有する。各爪状磁極23、24は、その先端を向かい合わせて交互に噛み合わせられるので、爪状磁極23、24の内周面23a、24aの傾斜が周

10

20

30

40

50

方向に互い違いで並ぶことになる。また、爪状磁極23、24の側面23c、24cは、根元側から先端側にいくにつれて先端側が細くなるように爪状磁極23、24の中心側に傾いている。

【0004】図18に示す如く、隣り合う爪状磁極23、24の間には、その対向する側面23c、24c同志で磁束の漏洩を減少する向きに着磁された直方体形状の磁石30Aが固定されている。

【0005】動作を以下に説明する。図外のバッテリからブラシ10、スリップリング9を通じてロータコイル13に電流が供給されて磁束が発生し、第1のポールコア体21の爪状磁極23にはN極が着磁され、第2のポールコア体22の爪状磁極24にはS極が着磁される。一方、エンジンの回転力によってブーリ4が回転され、シャフト6によってロータ7が回転するためステータコイル16には起電力が生じる。この交流の起電力は、整流器12を通って直流に整流されるとともに、レギュレータ20によりその大きさが調整されて、図外のバッテリに充電される。

【0006】上記磁石30Aは、爪状磁極23、24間に挿入される一体構成の直方体形状以外にも、一体構成のリング形状もしくは他の樹脂等でパッキングしたリング状のもの等、様々な形状、爪状磁極23、24に対する固定手段で設けられている。しかし、これらはつぎの問題が発生する場合がある。すなわち、製作時にどうしても磁石30Aに応力がかかったり、回転による遠心力が磁石30Aに加わってしまうので、耐久性に劣っていた。また、ポールコア体21、22は、一般的に鍛造によって製作されるので、特に複雑な形状である爪状磁極23、24の細部は、精度がそれほど高く出せない。また、爪状磁極23、24同士、固体間のばらつきが生じている。このようなばらつきのある爪状磁極23、24の内周面23a、24aに沿って、形状を合せた磁石30Aや、モールド等で形状を合せた支持部材は作りにくい。磁石30Aは、成形しやすさを考慮して製作すると、もろいので、ロータ7の爪状磁極23、24の周辺に用いるには、工夫が必要であった。しかし、磁石30Aに対して、厚みを十分にとったり、強度を重視した構成にすると、コストが高くなり量産には不都合であった。このようなばらつきに合せて磁石30Aや支持部材を製作し、爪状磁極23、24と磁石30A及び保持部材とのずれやギャップの差を小さくしたとする。しかし、この差がわずかであっても、ロータ7の回転時に遠心力を磁石30Aが受けると大きな力の差となり、磁石30Aや支持部材が損傷することが有り得る。また、爪状磁極23、24の内周面23a、24aに關係なく爪状磁極23、24の側面23c、24cで磁石30Aを支持したりする場合も、2個のポールコア体21、22を噛み合わせる際のずれや、回転力によるずれで、磁石30Aに力が加わる場合もあった。

〔0007〕一方、ロータ7の回転による遠心力や発電時のステータ8との磁気吸引力によって、各爪状磁極23、24は、その先端部がロータコイル13及びステータ8方向に往復する如く、それぞれ扇動する。これにより、爪状磁極23、24間の磁石30Aに荷重が加わって、磁石30Aに歪みが生じ、磁石30Aが破損することがあり得る。その対策の一例として、特開平11-136913に開示されたものがある。これは、図19ないし図20に示す如く、磁石30Bを構成する。すなわち、爪状磁極23、24毎に、爪状磁極23、24の内周面23a、24a及び側面23c、24c側を覆う如く構成して、磁石30Bを固着したものである。ここで、互いに隣り合う磁石30B、30B同志は、磁石間隙25を設けている。これよって、爪状磁極23と磁石30Bと、爪状磁極24と磁石30Bとがそれぞれ扇動するので、磁石30Bに荷重が加わらずに、磁石30Bの破損を防いでいる。

〔0008〕

〔発明が解決しようとする課題〕しかし、特開平11-136913号公報に開示されたものは、ロータ7の回転による遠心力の磁石30Bに対する影響軽減には無関係である。つまり、爪状磁極23、24と磁石30Bが一体になって扇動するが、爪状磁極23、24に比べて磁石30Bはもろいので、遠心力に対する耐久力が小さい。また、磁石30Bが完全に露出しているので、ケース3内に入り込んでしまった飛翔物によって損傷することが考えられる。さらに、磁石30Bの爪状磁極23、24への固定は、磁石30Bの凸凹で構成するので、回転に対して強度が不十分であった。また、磁石30Bにかかる遠心力を吸収するように、爪状磁極23、24の外周側にテープ等の支持部材を巻回して支持していた。しかし、これは回転中の動きまでは考慮していない、テープで適正な保持ができているとは限らなかった。つまり、ロータ7の回転により、支持部材の重みが磁石30Bにかかり、偏って支持したりしてしまい、高速回転時には磁石30Bのみならず、支持部材までも破壊してしまうおそれがあった。また、爪状磁極23、24の側面23c、24cが軸方向に対して傾いたり、径方向に対して傾いたりしていることで、取り付ける個々の磁石30B等も斜めとなる。磁石30Bを取り付ける際には、軸中心に向けて傾いたり外れたりすることもあり、仮止めが必要となったりし、作業に手間取っていた。組立て作業の手間としては、ロータコイル13を囲んで2つのポールコア体21、22を噛み合わせる際にも、いずれかの爪状磁極23、24の磁石30B等が抜け落ちる方向に向いてしまう。さらに、その後にシャフト6を取り付けて持ち運びする際にも、軸中心に向けて磁石30Bが落下する可能性があった。このとき、磁石30の爪状磁極23、24への仮止めとして相互間に接着剤を塗布した場合、一般的に接着する両面を近づける力を加

えた方が、乾燥、固定までの両者の位置関係を確保するにも良いことは周知である。この点、上記の構成の爪状磁極23、24と磁石30Bとでは、両者が離れる方向に力がかかりやすく、接着剤塗布工程にさらに保持工程が不可欠であり、作業が大変複雑になってコスト高となる恐れがあった。また、この際に不手際が発生していると、高温低温等の厳しい環境で長期に用いられる車両用交流発電機としてロータ構造を用いたとき、爪状磁極23、24と磁石30Bとの接着部が劣化を起こすことがあり、結果として磁石30が飛散する恐れもあった。

〔0009〕本発明は上記問題点を解消するためになされたもので、爪状磁極同志の磁束漏洩を減少する磁石に、ロータの回転時に加わる遠心力を低減するとともに、上記磁石を爪状磁極に取り付けることを目的とする。

〔0010〕

〔課題を解決するための手段〕この請求項1に係る発明は、磁束を発生するロータコイルと、このロータコイルを覆って設けられ、交互に噛み合うように突出される爪状磁極をそれぞれ有する第1のポールコア体及び第2のポールコア体から構成されたポールコアと、上記爪状磁極の両側面側に配設され、隣り合う爪状磁極の側面同志の磁束の漏洩を低減する磁石と、この磁石を外周側が互いに広がるように傾斜する如く支持する補強体とを備えたものである。

〔0011〕この請求項2に係る発明は、上記補強体は、爪状磁極の内周面に沿う内周部と、この内周部の両端から爪状磁極の側面へ折曲された折曲部と、この折曲部から折曲された磁石の外周面を押さえ付ける押さえ付け部と、押さえ付け部から磁石の外周面へ折返された折り返し部とより成り、補強体の内周側に上記磁石を支持したものである。

〔0012〕この請求項3に係る発明は、上記補強体は、爪状磁極の内周面と磁石の内周面に沿う内周部と、この内周部の両端から磁石の側面へ折曲された折曲部と、この折曲部から爪状磁極に突出して爪状磁極の外周面を押さえ付ける押さえ付け部とより成り、補強体の外周側に上記磁石を支持したものである。

〔0013〕この請求項4に係る発明は、上記磁石と補強体の磁石を支持した部分とにより側面磁石体を構成して、この側面磁石体と上記爪状磁極の側面との間に隙間を設け、上記磁石に遠心力が加わったときに、側面磁石体が爪状磁極側に上記隙間を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収するものである。

〔0014〕この請求項5に係る発明は、上記側面磁石体の回動中心は、ロータの回転軸中心と磁石の重心とを結ぶ線よりも爪状磁極側に位置され、上記側面磁石体の回動は、爪状磁極の側面に当接することで係止されるものである。

【0015】この請求項6に係る発明は、上記押さえ付け部と折り返し部とで磁石を支持して磁石とともに側面磁石体を構成し、この側面磁石体と上記爪状磁極の側面との間に隙間を設け、かつ隣り合う側面磁石体の相互間に隙間を設け、上記磁石に遠心力が加わったときに、側面磁石体が隣り合う側面磁石体側に上記側面磁石体相互間の隙間を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収し、上記側面磁石体の回動は、隣り合う保持部同志が当接して互いに係止し合うものである。

【0016】この請求項7に係る発明は、上記側面磁石体と上記爪状磁極の側面との間の隙間は、上記側面磁石体の回動が係止されて補強体の変形量が最大になってから上記磁石に遠心力が加わらなくなつたときに、変形した補強体が元の形状に戻るように、離間されたものである。

【0017】この請求項8に係る発明は、上記側面磁石体と上記爪状磁極の側面との間の隙間は、上記側面磁石体の回動が係止されて補強体の変形量が最大になつたときに補強体に加わる応力が、少なくとも許容応力以下となるように、離間されたものである。

【0018】この請求項9に係る発明は、上記側面磁石体と上記爪状磁極の側面との間の隙間には、弾性体を介在させたものである。

【0019】この請求項10に係る発明は、上記爪状磁極から補強体が内周側へ抜けることを防止する抜け止め構造を有するものである。

【0020】この請求項11に係る発明は、上記爪状磁極から補強体が先端側へ抜けることを防止する抜け止め構造を有するものである。

【0021】この請求項12に係る発明は、上記爪状磁極から補強体が内周側、先端側へ抜けることを防止する抜け止め構造を有するものである。

【0022】この請求項13に係る発明は、上記抜け止め構造は、上記補強体より突出して爪状磁極の外周面に当接する当接部であるものである。

【0023】この請求項14に係る発明は、上記抜け止め構造として、上記補強体を内周側から爪状磁極に押さえ付ける押さえ付け部材を用いたものである。

【0024】この請求項15に係る発明は、上記押さえ付け部材は、円筒状の外周面を有し、この外周面には補強体が組付けられた爪状磁極がはまる溝が形成され、爪状磁極の外周面と共にロータの外周面に円筒状の曲面を構成するものである。

【0025】この請求項16に係る発明は、上記爪状磁極の側面は、内周側よりも外周側に広がる向きに傾いた傾斜角度を有するものである。

【0026】この請求項17に係る発明は、上記磁石の重心は、爪状磁極の根元側に片寄って配置されるものである。

【0027】この請求項18に係る発明は、上記補強体は、金属製であるものである。

【0028】この請求項19に係る発明は、上記補強体は、爪状磁極に溶接で固定されるものである。

【0029】この請求項20に係る発明は、上記補強体は、磁石が補強体の先端側、根元側へ抜けることを防止する抜け止め構造を有するものである。

【0030】

【発明の実施の形態】以下、本発明の実施の形態について図面に基づき説明する。

【0031】実施の形態1. 図1ないし図3は、本発明の実施の形態1に係わるロータ構造を車両用交流発電機のロータに用いた場合を示し、図1は車両用交流発電機のロータの構成を示す要部斜視図、図2は分解斜視図、図3は補強体の断面図であり、図17ないし図20と同じものは同一符号を用いている。図1に示す如く、爪状磁極23、24同志の漏洩磁束を低減するように着磁されたフェライト磁石30が、各爪状磁極23の両側面23c、23cに2つづ、各爪状磁極24の両側面24c、24cに2つづ配置される。この磁石30は、ロータ7の回転時に上記磁石30に加わる遠心力を、自身の変形により吸収する補強体40によって、外周側が互いに広がるように傾斜する如く、爪状磁極23、24に支持されている。補強体40は、厚み0.5mm程度のステンレス鋼等の金属プレートより成り、1枚の金属板をプレス加工により折り曲げて形成するので、容易に製作できる。この補強体40は、図2ないし図3に示す如く、ロータ7の軸方向に対する断面が略M字形状であり、爪状磁極23、24の内周面23a、24aに沿う台形板状の内周部40aと、この内周部40aの両端から外径側に折曲し、爪状磁極23、24の両側面23c、24cに沿う折曲部40bと、折曲部40bの先端から磁石30の外周面に折曲し、この外周面を押さえ付ける押さえ付け部40cと、押さえ付け部40cから磁石30の側面側に折返される折り返し部40dとより成る。これらの折曲部40b、押さえ付け部40c、折り返し部40dで磁石30を外周側から取り囲むとともに、折曲部40bと折り返し部40dで磁石30を外周側から挟み込んで補強体40の内周側に保持している。

【0032】図3に示す如く、上記内周部40aとその両端の折曲部40b、40bは、内周側の長さQと比べて外周側の長さPが広くなるように、折曲部40b、40bの先端側が広がっており、ほぼU字状に形成される。磁石30を囲んだ補強体40の折曲部40b、押さえ付け部40c、折り返し部40dは、磁石30の断面外形に沿う逆U字状である。すなわち、磁石30は、爪状磁極23、24の側面23c、24cに、ロータ7の回転軸中心7pを通る爪状磁極23、24の中心線から外周面23b、24b側に広がる向きに傾けて設けられている。磁石30は、図2に示す如く、爪状磁極23、

24との保持部を設ける必要がなく、その側面30cは爪状磁極23、24の側面23c、24cに沿った台形である。幅はほぼ一定であり、厚みが爪状磁極23、24の形状に合せて、先端側30sから根元側30nへ太くなる截頭四角錐形である。また、磁石30は直方体状であってもよい。このように磁石30を補強体40に保持して、爪状磁極23、24に固定するためには、接着剤等が用いられる。つまり、補強体40の内周部40aと爪状磁極23、24の内周面23a、24aとの境界部分、補強体40の折曲部40b、押さえ付け部40c、折り返し部40dと磁石30との境界部分に、接着剤が塗布される。爪状磁極23、24に固定する際には、爪状磁極23、24の側面23c、24cと補強体40の折曲部40bと間には、間隙として微小空間Sを有して互いに離れて組付けられる。

〔0033〕この構成により、図3におけるロータ7の回転時に磁石30の重心30jに加わる遠心力30Eは、磁石30と補強体40の磁石30が保持された部分を回動させる力(モーメント)となって、補強体40に吸収される。上記磁石30及び補強体40の磁石30が保持された部分(折曲部40b、押さえ付け部40c、折り返し部40d)を、側面磁石体50として呼ぶことにして、図3を用いて側面磁石体50に加わるモーメントを説明する。すなわち、側面磁石体50は、その支点Hが補強体40の内周部40aの両端にあり、いわゆる片持ち支持される。つまり、支点Hはロータ7の回転軸中心7pと磁石30の重心30jとを結ぶ線より爪状磁極23、24側に位置している。これにより、磁石30へ加わる遠心力30Eが、上記モーメントとして補強体40に加わることになる。側面磁石体50に加わる上記モーメントの方向は、回動中心が支点Hとなり、補強体40の中心方向、つまり爪状磁極23、24の中心方向となる。従って、上記モーメントにより側面磁石体50は、その外径側が爪状磁極23、24の側面23c、24cに近づくように回動して変位する。この変位により補強体40に応力が加わるが、この応力が許容応力以下となるように、上記微小空間Sが離間されており、補強体40は破損しない。この場合、微小空間Sは、補強体40が変位した後に、磁石30に遠心力30Eが加わらなくなったりときに、補強体40が元の形状に戻る程度の間隙である。これにより、補強体40は、爪状磁極23、24を挟持するので保持力が高まり、結果として磁石30と爪状磁極23、24との一体化が促進される。また、ロータ7の回転時に爪状磁極23、24の先端側が、内周側及び外周側に振動したときに、補強体40のスプリングバック等により、側面磁石体50の先端が広がることが考えられる。しかし、上記モーメントによる側面磁石体50の変位は、上記スプリングバックを相殺する方向であり、磁石30及び補強体40が爪状磁極23、24から脱落するなどの不具合が回避できる。

〔0034〕また、爪状磁極23、24の内周面23a、24aが補強体40の内周部40aに接しているため、発電時に爪状磁極23、24に伝導された熱が補強体40によって放熱される。しかし、本実施の形態1の主としての目的は、磁石30に加わる遠心力30Eを低減させることである。この補強体40に保持された磁石30は、ロータコイル13に対向する内径面側が露出しており、発電時に発生した熱が放熱される。残る3面は、ほぼ補強体40で囲まれており、耐遠心力性が高い。万が一に飛翔物が外径側からぶつかったとしても、補強体40で覆われているので磁石30が損傷するおそれもない。爪状磁極23、24への装着時には、磁石30が補強体40で覆われた状態で組付けられ、かつ磁石30と爪状磁極23、24が接する面がないため、組立て作業時に磁石30が欠損することがない。爪状磁極23、24は、側面23c、24cに補強体40がはめ込まれる切り欠きが形成されるが、先端部が細くなる形状は従来例と同じである。従って、爪状磁極23、24の側面23c、24c相互間で形成される空間は、外周視で略平行4辺形となる。この個々の爪状磁極23、24の側面23c、24cに、磁石30が固着された補強体40を組付けて、補強体40同志で形成される空間は、巾は狭くなるが同じく略平行4辺形となる。これによって、爪状磁極23、24の先端がロータ7の回転時に扇動しても、磁石30に応力が加わらずに破壊もしなくなる。

〔0035〕また、補強体40は接着材等を介して爪状磁極23、24に固着したが、補強体40は金属製であるので、爪状磁極23、24の内周面23a、24aと補強体40の内周部40aとを溶接で接合しても良い。また、爪状磁極23、24の両側面23c、24cと補強体40の折曲部40bとの間隙には、微小空間Sが設けられているが、この微小空間Sにゴムや樹脂等の弾性体を封入して介在させるようにしてもよい。形状としては、微小空間Sに合う三角柱状、薄板状や棒状等の挿入し易い形状とする。これによれば、同様の効果が得られるとともに、さらにこの弾性体が衝撃力を吸収するとともに、異物混入を抑えることもできる。

〔0036〕実施の形態2、上記実施の形態1は、補強体40の断面形状が略M字状であった場合を説明したが、この実施の形態2は、図4ないし図5に示すように、断面形状が略C字状の補強体41を用いている。図5に示す如く、補強体41は、爪状磁極23、24の内周面23a、24aに沿って磁石31の内周面まで延長された台形板状の内周部41aと、内周部41aの両端から外径方向に折曲されて磁石31の側面を保持する折曲部41bと、折曲部41bの先端から爪状磁極23、24方向に突出し、磁石31を内周側に押さえ付ける押さえ付け部41cとより成る。押さえ付け部41cは、磁石31の外周側全面を覆う必要がなく、半分強を占め

る程度で磁石31の保持確保ができる程度に、爪状磁極23, 24の途中まで突出している。押さえ付け部41cと爪状磁極23, 24との間にはギャップがあり、磁石31の外周側の一部が露出されている。この補強体41の折曲部41bと爪状磁極23, 24の側面23c, 24cとて磁石31を内周側より挟み込んで、磁石31を補強体41の外周側に保持して爪状磁極23, 24に支持している。押さえ付け部41cは、磁石31の根元部が太くなっていることから、内周部41aで磁石31をくさびのように挟むことになり、爪状磁極23, 24の先端から磁石31が抜けることを防止するものである。

【0037】上記磁石31の3面は、ほぼ補強体41で取り囲まれ、残る1面は爪状磁極23, 24の側面23c, 24cに接するので、大きな露出面がなく、耐久性が高い。また、磁石31は実施の形態1の磁石30と比較すると、太幅のものを用いることができる。すなわち、爪状磁極23, 24相互間に注目すると、補強体41には補強体40の折り返し部40dに相当する部分を設ける必要がなく、周方向に対して補強体41の板厚の占める割合が半分となる。そのため、磁石30と比べて、その厚み分大きな磁石31となり、さらに車両用交流発電機の出力が上昇することになる。実施の形態1と同様に、爪状磁極23, 24の側面23c, 24cと磁石31との間隙には、微小空間Sを有して離れており、その他の部分が接着材等で固定される。つまり、磁石31と補強体41の折曲部41b、押さえ付け部41cとの境界部分に接着剤が塗布されて、これらが側面磁石体51を構成する。磁石31の重心31jに加わる遠心力31Eのモーメントを考えると、実施の形態1と同様である。すなわち、側面磁石体51は、爪状磁極23, 24の内周面23a, 24aと側面23c, 24cの角部に当たる内周部41aの支点Hが回動中心となり、爪状磁極23, 24の中心方向に変位する。実施の形態1とは異なる点は、磁石31が補強体41の外周側に配置されるので、補強体41の内周部41aは、磁石31の内周面を覆う分長さが内周部40aより長くなり、補強体41のスプリングバックを相殺する力が増強される。これにより、磁石31の脱落防止を促進するとともに、さらに爪状磁極23, 24と磁石31とが一体化される。また、図6に示す如く、補強体41の内周部41aの上、下両端を折曲して抜け止め部41n, 41nを設けてもよい。これにより、磁石31が補強体41の先端側、根元側から抜け落ちることを確実に防止できる。抜け止め部41nは、折曲部41bの上、下両端に設けてもよい。

【0038】実施の形態3。上記実施の形態1は、爪状磁極23, 24の側面23c, 24cと補強体40の折曲部40bとの間に微小空間Sを設けた場合を説明したが、この実施の形態3は、図7(a), (b)に示すよ

うに、磁石30は、押さえ付け部40cと折り返し部40dとに接着されている。この押さえ付け部40c、折り返し部40d、磁石30で側面磁石体50を構成する。そして、隣り合う側面磁石体50相互の間隙に微小空間Uを設け、さらに、補強体40の折曲部40bと磁石30の側面との間隙に、微小空間Tを設けるものである。この場合は、側面磁石体50の回動中心が異なり、折曲部40bの外周先端が支点Jとなり、片持ち支持となる。磁石30の重心に加わる遠心力のモーメントによる側面磁石体50の変位は、実施の形態1とは逆方向となる。すなわち、隣り合う補強体40の折り返し部40d同志が近づく方向、つまり爪状磁極23, 24の周方向中心側に向いて、微小空間Uを狭めるように側面磁石体50が隣り合う側面磁石体50側に回動する。この場合の上記微小空間Sは、設けなくともよいが、微小空間Sを設ける場合には接着材で固定してもよく、樹脂等の弾性体を充填して介在させるようにしてもよく、微小空間Tより小さければよい。これにより、図7(b)に示すように、ロータ7の回転時に側面磁石体50の内周側は、周方向に微小空間Uを狭める方向に変位するので、同様にして隣りの側面磁石体50が微小空間Uを狭める方向に変位する。すると、補強体40の折り返し部40d同志が当接して、側面磁石体50同志が互いに支持し合うことになる。こうすることで、不要な変位が抑えられるので、高速回転時の耐遠心力性も向上できる。また、補強体40同志が当接するので、磁石30には影響を与えない。また、回動中心となる支点Jから爪状磁極23, 24側の補強体40の折曲部40bには影響を与えない。

【0039】実施の形態4。上記実施の形態2は、補強体41の押さえ付け部41cは磁石31の外周面の途中まで突出した場合を説明したが、この実施の形態4は、図8ないし図9に示すように、押さえ付け部41cの上、下端から爪状磁極23, 24の外周面23b, 24bの一部まで突出する細幅の当接部41t, 41tを構成したものである。なお、図9(a), (b)は、それぞれ図8におけるB-B線、A-A線断面視に相当する断面図である。当接部41tは、爪状磁極23, 24の外周面23b, 24bの周方向両端に形成される面取り部23m, 24mの途中まで突出して係止されるので、爪状磁極23, 24から補強体41が内周方向へ抜けることを防止する。これは、爪状磁極23, 24に対しては、追加の加工は不要である。しかし、設計上の理由により加工を施した場合でも、当接部41tの板厚分のわずかな加工で良く、磁気回路への影響は無視できる。また、当接部41tは補強体41の押さえ付け部41cの軸方向両端から一部が突出しているので、磁石31の露出面積は確保されており、冷却性を低下させない。この構成によれば、爪状磁極23, 24に接着材を介して補強体41及び磁石31を取り付ける際には、治具によっ

て個々を保持する必要がなくなり、大幅なコストダウンが可能となる。そればかりでなく、経年によって接着剤が劣化すること等を考慮しても、補強体41の当接部41tと内周部41aが爪状磁極23, 24を挿し続けるため、保持力を失はないので、高信頼性、高品質の製品が得られる。また、補強体40に当接部を設ける場合には、押さえ付け部40cの上、下端の一部を爪状磁極23, 24の外周面23b, 24b側に折返すことで形成できる。また、当接部は、押さえ付け部40c, 41cに板状の当接片を固着して設けてもよい。

【0040】実施の形態5. 上記実施の形態4は、爪状磁極23, 24の面取り部23m, 24mには加工を施さなかつたが、この実施の形態5では、図10ないし図11に示す如く、面取り部23m, 24mの当接部41t, 41tに対応する部分に、わずかにへこませた凹状の段部23h, 24hを設けたものである。この段部23h, 24hは、当接部41tの軸方向の移動を規制するものであり、補強体41が爪状磁極23, 24の先端から抜けることを防止する。なお、図11(a)、

(b)は、それぞれ図10におけるC-C線、A-A線断面視に相当する断面図である。この段部23h, 24hは、爪状磁極23, 24に対して補強体41を装着した際に、爪状磁極23, 24の外周面23b, 24bと当接部41tとがほぼ平らになるように形成されている。この段部23h, 24hに当接部41tがはまりこむことで、補強体41つまりは磁石31が爪状磁極23, 24とが一体化されて形成される。そのため、組付けた後の全体の外周面としては、なだらかな曲面になって空気抵抗が減少し、回転抵抗を悪化させない。この段部23h, 24hは、爪状磁極23, 24の面取り部23m, 24mの一部の形状を若干変更するだけで対応可能であり、別部材を追加する必要がない。この段部23h, 24hは、ポールコア体21, 22を形成する型で構成するようにしてもよく、面取り部23m, 24mに加工して設けてもよい。また、わずかにへこませるだけなので、爪状磁極23, 24に対して磁気的に影響を及ぼすことはない。結果としては、爪状磁極23, 24への固定のための接着材が不要となり、さらに安価となり、かつ製作も容易となる。

【0041】実施の形態6. 上記実施の形態2は、補強体41は接着剤のみで爪状磁極23, 24に固定されていたが、この実施の形態6は、図12に示す如く、補強体41を内周側から爪状磁極23, 24に押さえ付けるリング状の押さえ付け部材60を用いるものである。これは、補強体41が爪状磁極23, 24の内周側または先端側から抜けることを防止する。実施の形態4, 5と比べると、さらに補強体41の爪状磁極23, 24への保持度が高まることになる。図12(a)に示す如く、それぞれの爪状磁極23, 24の所定位置に、磁石31を保持した補強体41を配置した後に、図12(b)、

(c)に示す如く、補強体41の内周部41aの中央部付近に当接する直径を有する押さえ付け部材60をはめこんで構成する。この押さえ付け部材60は、補強体41の内周部41aの軸方向傾斜に合った傾きを外周面に有したものであり、接着面積が大きく密着度が高い。これにより、爪状磁極23, 24に補強体41を取り付けた状態で確実に保持でき、その後の持ち運びにも優れる。また、複数の補強体41を爪状磁極23, 24に対して一度に固定でき、補強体41の構成も単純なもの可能となる。押さえ付け部材60は、金属又はプラスチック等より成り、断面は長方形であってもよい。また、爪状磁極23, 24と補強体41の両者間に接着材を設けてあれば、接着面を近づける方向となり、余分な保持は不要となり、かつ接着強度が確保される。また、複数の補強体41および磁石31を押さえ付け部材60とそろえて、組立て時の治具により保持して、これを爪状磁極23, 24と一体化させるのであれば、接着材の固定はしなくても良い。また、上記押さえ付け部材60は、補強体40も使用でき、内周部40aが押さえつけられる。

【0042】実施の形態7. 実施の形態6は、押さえ付け部材60の外周は補強体40, 41の内周部40a, 41aに当接したが、この実施の形態7は、図13ないし図14に示す如く、リング状の押さえ付け部材70は、ロータ7の外周と同一の円筒状の外周面70bを有し、この外周面70bには補強体40が組付けられた爪状磁極23, 24がはまる凹状の溝70mが形成されるものである。図14に示す如く、ロータ7として組付けたときに、爪状磁極23, 24の外周面23b, 24bと共にロータ7の外周面がほぼ完全な円筒状の曲面を構成する。図13に示す如く、押さえ付け部材70の内周側は、ロータコイル13との間に隙間があり、冷却風70Fが通過してロータ7が冷却される。これにより、補強体40が軸方向に幅広の押さえ付け部材70で内周側から外周側に押さえられるので、実施の形態6と比べて、さらに確実に爪状磁極23, 24と一体化できる。さらに、外周面70bに円筒状曲面を有することで、複数の磁石30を有するロータ7であっても回転による風音を悪化させない効果も有する。なお、押さえ付け部材70の幅は、爪状磁極23, 24の先端を覆う程度であったが、ポールコア体21, 22の基部21k, 22kの端面まで突出する程度の幅を有してもよい。

【0043】実施の形態8. この実施の形態8は、図15(a), (b)に示すように、爪状磁極23, 24の側面23c, 24cの傾斜角度を、爪状磁極23, 24の内周面23a, 24aより外周面23b, 24b側がさらに広がるように形成したものである。この傾斜角度がきつくなつた側面23c, 24cに沿って、補強体40, 41が形成されている。これによれば、磁石30, 31の内周側の先端は、外周視で見えにくくなり、あた

かも爪状磁極23, 24の内周面23a, 24a側にもぐりこむように配置されることになる。このようにすれば、磁石30, 31単体に加わる遠心力30E, 31Eは、2つの力に分散される。すなわち、側面23c, 24cに対して垂直方向に加わる抗力30K, 31Kが増加し、側面23c, 24cに対して水平外周方向に加わる分散力30B, 31Bが減少する。そのため、側面磁石体50, 51の耐遠心力性が向上する。

【0044】実施の形態9。この実施の形態9は、図6に示すように、周方向断面視で磁石30, 31は、根元側30n, 31nが先端側30s, 31sより太くなる形状で設けられる。図は補強体40, 41等が省略され、爪状磁極23, 24の周方向断面視で磁石30, 31の形状を示している。すなわち、磁石30, 31の重心は、爪状磁極23, 24の先端側より根元側、つまりポールコア体21, 22の基部21k, 22k側に片寄ることになる。このようにすれば、爪状磁極23, 24に磁気吸引力を受けたり、ロータ7の回転による遠心力によって爪状磁極23, 24の先端が扇動するが、この変位が低減できる。つまり、磁石30, 31へ影響する力も低減できる。

【0045】

【発明の効果】以上説明したように、請求項1に記載の発明によれば、磁束を発生するロータコイルと、このロータコイルを覆って設けられ、交互に噛み合うように突出される爪状磁極をそれぞれ有する第1のポールコア体及び第2のポールコア体から構成されたポールコアと、上記爪状磁極の両側面側に配設され、隣り合う爪状磁極の側面同志の磁束の漏洩を低減する磁石と、この磁石を外周側が互いに広がるように傾斜する如く支持する補強体とを備えたので、磁石を補強体で囲んだ状態で個々の爪状磁極に確実に固定でき、磁石に工夫をしなくとも、磁石及び補強体の磁石が保持された部分より成る側面磁石体の強度を高くでき、耐遠心力性も高い。

【0046】また、請求項2に記載の発明によれば、上記補強体は、爪状磁極の内周面に沿う内周部と、この内周部の両端から爪状磁極の側面へ折曲された折曲部と、この折曲部から折曲された磁石の外周面を押さえ付ける押さえ付け部と、押さえ付け部から磁石の外周面へ折返された折り返し部とより成り、補強体の内周側に上記磁石を支持したので、製作が容易で安価なものができ、補強体自体の強度も高く、また爪状磁極の内周面と側面とに補強体が連続して設けられるので、遠心力や爪状磁極にかかる扇動力を内周側から全面で受けることができ、磁石に影響する力を軽減できる。

【0047】また、請求項3に記載の発明によれば、上記補強体は、爪状磁極の内周面と磁石の内周面に沿う内周部と、この内周部の両端から磁石の側面へ折曲された折曲部と、この折曲部から爪状磁極に突出して爪状磁極の外周面を押さえ付ける押さえ付け部とより成り、補強

体の外周側に上記磁石を支持したので、製作が容易で安価なものが得られるとともに、爪状磁極の内周面と磁石の内周面とに補強体が連続して設けられるので、遠心力や爪状磁極にかかる扇動力を内周側から全面で受けることができ、磁石に影響する力を軽減できる。

【0048】また、請求項4に記載の発明によれば、上記磁石と補強体の磁石を支持した部分により側面磁石体を構成して、この側面磁石体と上記爪状磁極の側面との間に間隙を設け、上記磁石に遠心力が加わったときに、側面磁石体が爪状磁極側に上記間隙を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収するので、ロータの回転により遠心力が発生しても、上記側面磁石体が爪状磁極を扶持するように、個々の爪状磁極の中心方向側に向かって回動して変位するために、補強体の保持力が強化され、耐遠心力性も高い。

【0049】また、請求項5に記載の発明によれば、上記側面磁石体の回動中心は、ロータの回転軸中心と磁石の重心とを結ぶ線よりも爪状磁極側に位置され、上記側面磁石体の回動は、爪状磁極の側面に当接することで係止されるので、遠心力が増加しても側面磁石体が確実に固定され、さらなる変位を抑制でき、磁石に遠心力が加わらずに耐遠心力性が高い。

【0050】また、請求項6に記載の発明によれば、上記押さえ付け部と折り返し部とで磁石を支持して磁石とともに側面磁石体を構成し、この側面磁石体と上記爪状磁極の側面との間に間隙を設け、かつ隣り合う側面磁石体の相互間に間隙を設け、上記磁石に遠心力が加わったときに、側面磁石体が隣り合う側面磁石体側に上記側面磁石体相互間の間隙を狭めるように回動し、この回動力により補強体が変形して上記遠心力を補強体で吸収し、上記側面磁石体の回動は、隣り合う保持部同志が当接して互いに係止し合うので、遠心力が増加しても側面磁石体が確実に固定され、さらなる変位を抑制でき、磁石に遠心力が加わらずに耐遠心力性が高い。

【0051】また、請求項7に記載の発明によれば、上記側面磁石体と上記爪状磁極の側面との間の間隙は、上記側面磁石体の回動が係止されて補強体の変形量が最大になってから上記磁石に遠心力が加わらなくなつたときに、変形した補強体が元の形状に戻るよう、離間されたので、再び遠心力が加わったときに、側面磁石体が回動でき、補強体が破損することなく回動動作を繰返すことができる。

【0052】また、請求項8に記載の発明によれば、上記側面磁石体と上記爪状磁極の側面との間の間隙は、上記側面磁石体の回動が係止されて補強体の変形量が最大になつたときに補強体に加わる応力が、少なくとも許容応力以下となるように、離間されたので、側面磁石体が回動して最大に変位しても、補強体の変形量は許容以下となり、過大な応力で補強体が破損することがない。

【0053】また、請求項9に記載の発明によれば、上記側面磁石体と上記爪状磁極の側面との間の隙間に、弾性体を介在させたので、隙間に有しても異物がはさまったりせず、また、上記側面磁石体の変位時に爪状磁極との衝撃力を緩和できる。

【0054】また、請求項10に記載の発明によれば、上記爪状磁極から補強体が内周側へ抜けることを防止する抜け止め構造を有するので、補強体と爪状磁極との一体化が高まり、磁石が飛散せずに損傷を防止できるとともに、補強体を組付けたポールコア体を軸方向に対して水平にしても、補強体が内周側に抜けてしまうことがないため、持ち運びやセッティングの自由度も高く、作業性に優れる。

【0055】また、請求項11に記載の発明によれば、上記爪状磁極から補強体が先端側へ抜けることを防止する抜け止め構造を有するので、補強体と爪状磁極との一体化が高まり、磁石が飛散せずに損傷を防止でき、また、補強体が爪状磁極から軸方向に抜け落ちることがなく、補強体を取り付けたポールコア体同志を、ロータコイルを内包して容易に対応に噛み合わせることができる。

【0056】また、請求項12に記載の発明によれば、上記爪状磁極から補強体が内周側、先端側へ抜けることを防止する抜け止め構造を有するので、簡単な構成で爪状磁極に対する補強体の内周方向、軸方向への移動を確実に規制でき、保持機能が高い。

【0057】また、請求項13に記載の発明によれば、上記抜け止め構造は、上記補強体より突出して爪状磁極の外周面に当接する当接部であるので、簡単な構成で爪状磁極の面取り部を挟持して、爪状磁極の内周方向へ対する補強体の抜け止め効果を有することができる。

【0058】また、請求項14に記載の発明によれば、上記抜け止め構造として、上記補強体を内周側から爪状磁極に押さえ付ける押さえ付け部材を用いたので、爪状磁極に対する補強体の内周方向、軸方向内周方向、軸方向への移動を規制するとともに、補強体に対して内周側から爪状磁極に向かって押し付ける力を附加できる。

【0059】また、請求項15に記載の発明によれば、上記押さえ付け部材は、円筒状の外周面を有し、この外周面には補強体が組付けられた爪状磁極がはまる溝が形成され、爪状磁極の外周面と共にロータの外周面に円筒状の曲面を構成するので、爪状磁極に対する補強体の内周方向、軸方向内周方向、軸方向への移動をさらに確実に規制でき、また、ロータの外周全体として滑らかな曲面となり、ロータの回転時に発生する風音が低減される。

【0060】また、請求項16に記載の発明によれば、上記爪状磁極の側面は、内周側よりも外周側に広がる向きに傾いた傾斜角度を有するので、爪状磁極の側面に垂直に加わる抗力が増加し、磁石単体に加わる遠心力が低減され、側面磁石体の耐遠心力性が向上する。

【0061】また、請求項17に記載の発明によれば、上記磁石の重心は、爪状磁極の根元側に片寄って配置されるので、ロータの回転時に爪状磁極の先端が扇動しても、この振幅量を低減できる。

【0062】また、請求項18に記載の発明によれば、上記補強体は、金属製であるので、工作自由度が高く、安価に製作できる。

【0063】また、請求項19に記載の発明によれば、上記補強体は、爪状磁極に溶接で固定されるので、補強体と爪状磁極を確実に一体化できる。

【0064】また、請求項20に記載の発明によれば、上記補強体は、磁石が補強体の先端側、根元側へ抜けることを防止する抜け止め構造を有するので、補強体からの磁石の脱落を防止できる。

【図面の簡単な説明】

【図1】 本発明の実施の形態1に係わるロータ構造の構成を示す要部を示す斜視図である。

【図2】 実施の形態1に係わるロータ構造の要部を示す分解斜視図である。

20 【図3】 実施の形態1に係わる補強体、磁石を示す爪状磁極の軸方向視の断面図である。

【図4】 実施の形態2に係わるロータ構造の構成を示す要部を示す斜視図である。

【図5】 実施の形態2に係わる補強体、磁石を示す爪状磁極の軸方向視の断面図である。

【図6】 実施の形態2に係わる補強体の抜け止め部を示す斜視図である。

【図7】 実施の形態3に係わる補強体、磁石を示す爪状磁極の軸方向断面視の動作説明図である。

30 【図8】 実施の形態4に係わる当接部を示す側面視概略図である。

【図9】 実施の形態4に係わる当接部、補強体、磁石を示す爪状磁極の軸方向視の断面図である。

【図10】 実施の形態5に係わる段部を示す側面視概略図である。

【図11】 実施の形態5に係わる段部、当接部、補強体、磁石を示す爪状磁極の軸方向視の断面図である。

【図12】 実施の形態6に係わる押さえ付け部材を補強体に装着した状態を説明する平面図である。

40 【図13】 実施の形態7に係わる押さえ付け部材を示す軸方向視の断面図である。

【図14】 実施の形態7に係わる押さえ付け部材、ロータを示す側面図である。

【図15】 実施の形態8に係わる爪状磁極の側面、補強体、磁石を示す軸方向視の断面図である。

【図16】 実施の形態9に係わる磁石の形状を示す爪状磁極の周方向視の断面図である。

【図17】 従来のロータ構造を説明する車両用交流発電機の構成を示す断面図である。

50 【図18】 従来のロータ構造を説明する斜視図であ

る。

【図19】 従来のロータ構造を説明する斜視図である。

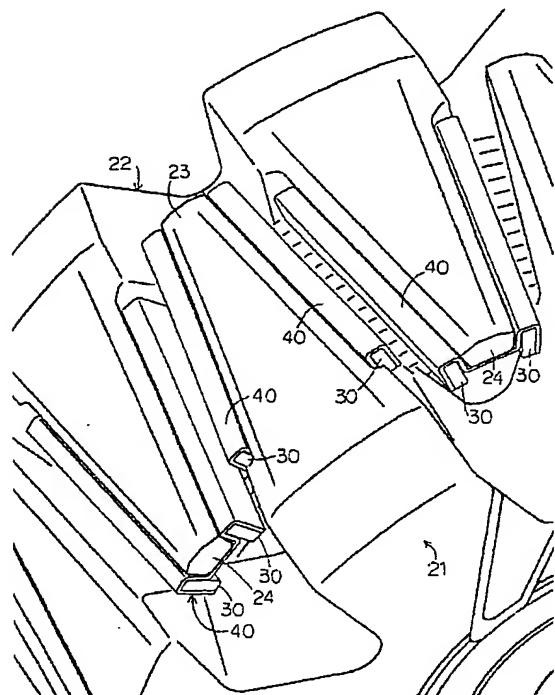
【図20】 従来のロータ構造を説明する分解側面図である。

【符号の説明】

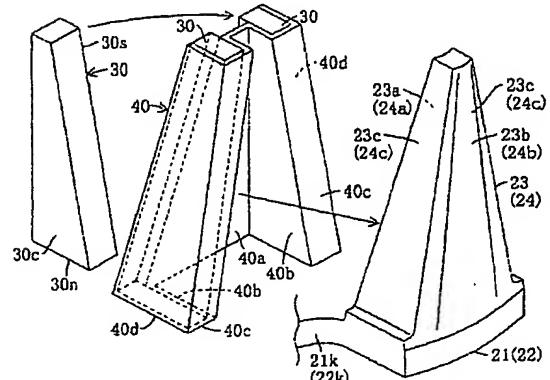
* 23, 24 爪状磁極、23a, 24a 内周面、23c, 24c 側面、30, 31 磁石、40, 41 補強体、40a, 41a 内周部、40b, 41b 折曲部、40c, 41c 押さえ付け部、40d 折り返し部、50, 51 側面磁石体。

*

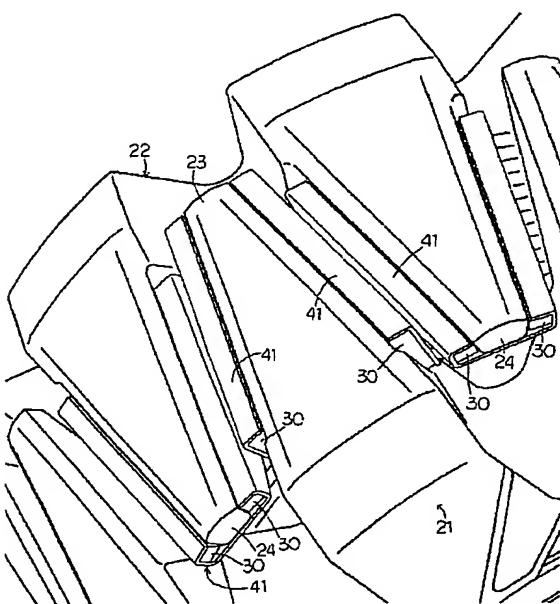
【図1】



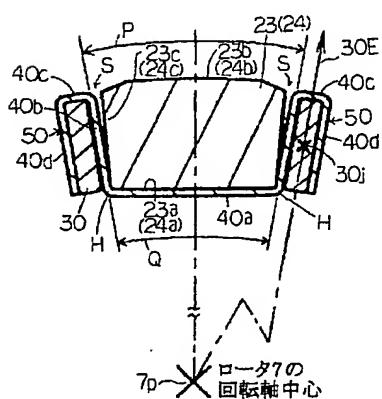
【図2】



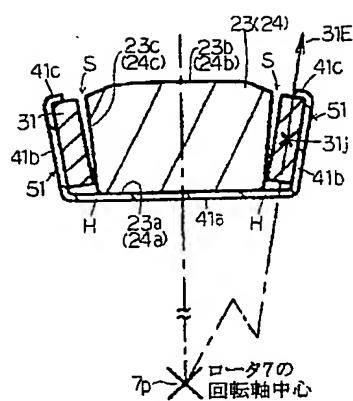
【図4】



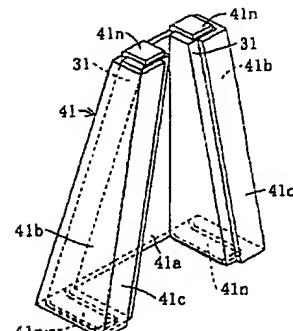
【図3】



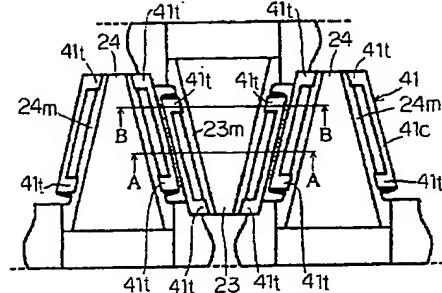
[图5]



[図6]

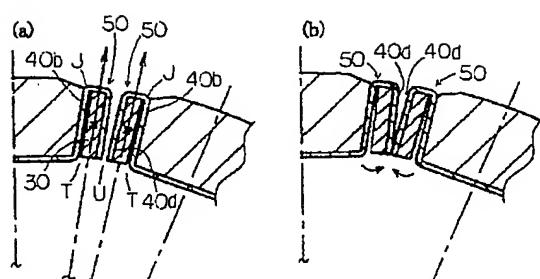


[図8]

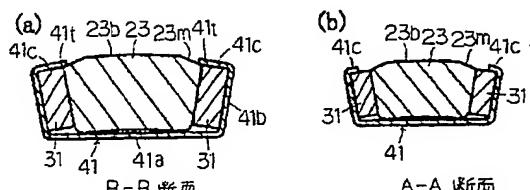


[図9]

[図7]

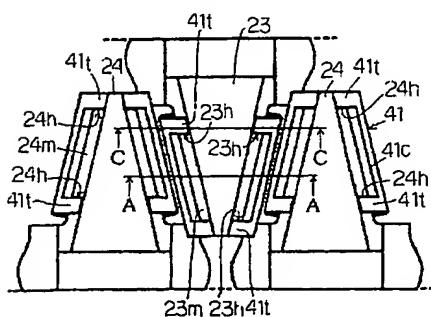


ロータの 回転軸中心

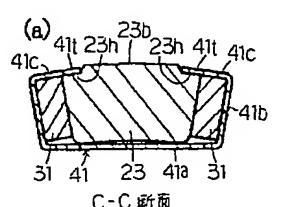


A-A 断面

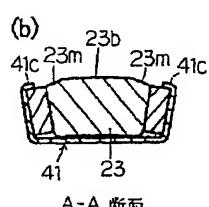
[圖 10]



[図11]



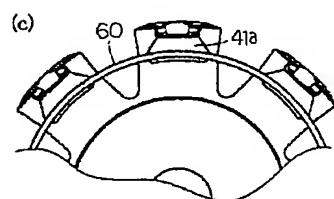
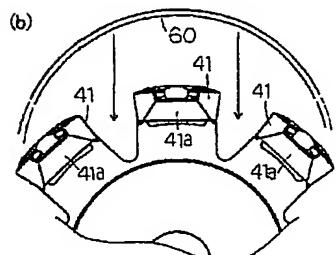
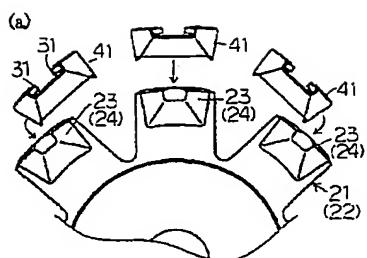
C-C 斷面



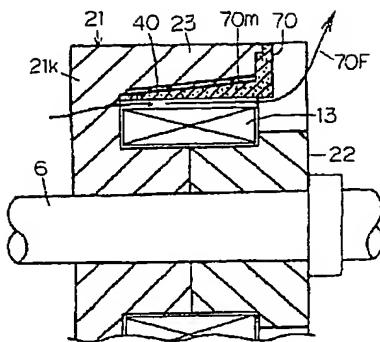
A-A 断面

(13)

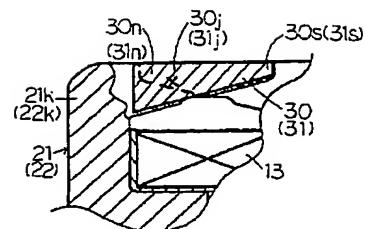
[図12]



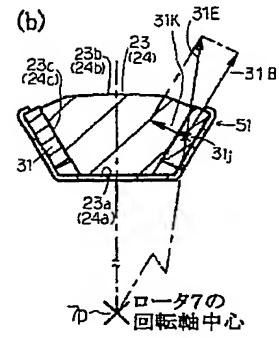
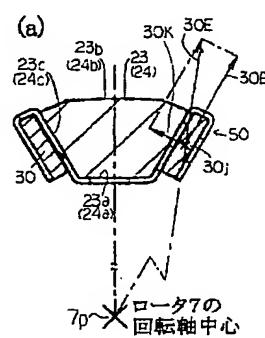
[図13]



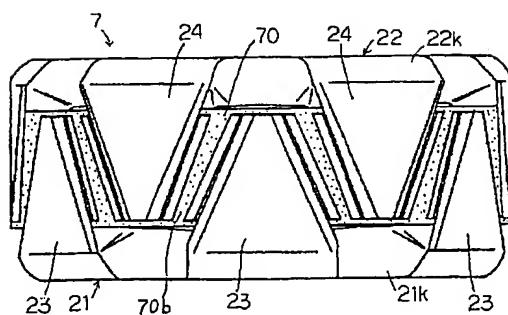
[図16]



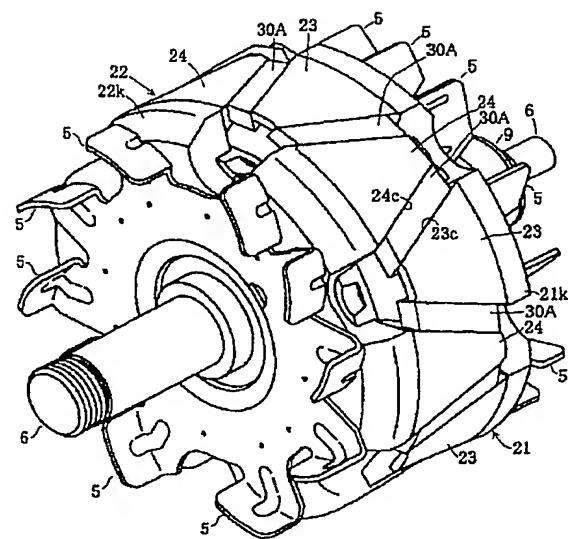
[図15]



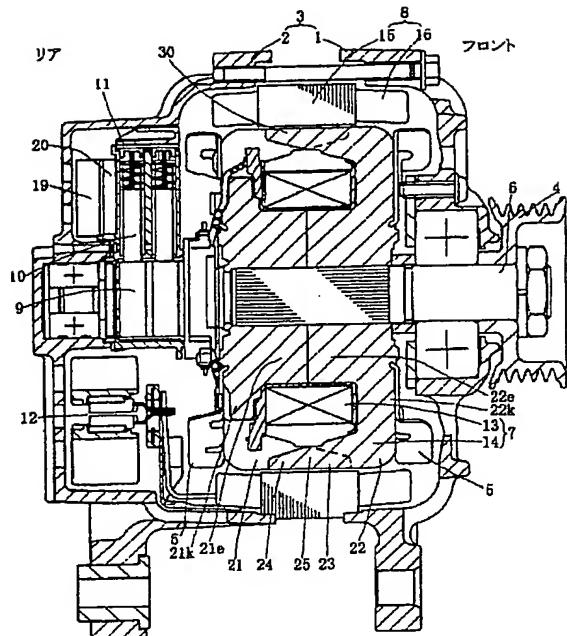
[図14]



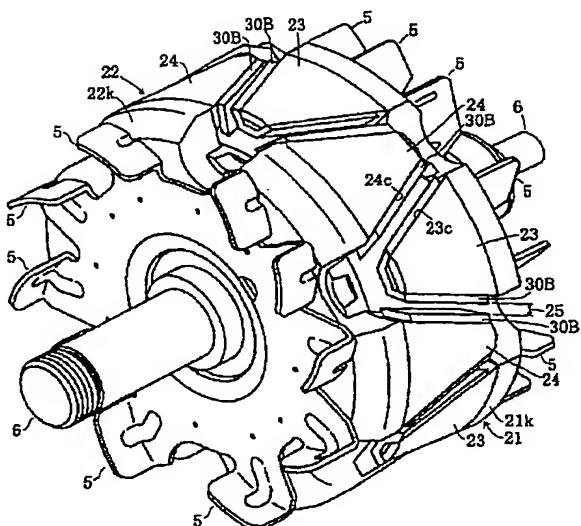
[図18]



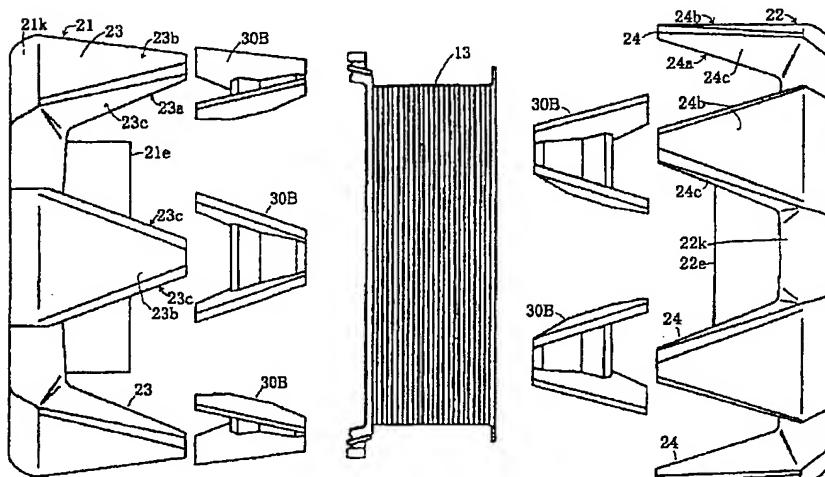
〔図17〕



[図19]



(图20)



フロントページの続き

(72)発明者 鶴原 健二
東京都千代田区丸の内二丁目2番3号 三
菱電機株式会社内

(72)発明者 大橋 篤志
東京都千代田区丸の内二丁目2番3号 三
菱電機株式会社内

F ターム(参考) 5H619 AA03 AA07 BB02 BB17 PP02
PP04 PP08



05.6.24
特許事務所

(12) United States Patent
Higashino et al.



US006201335B1

(10) Patent No.: US 6,201,335 B1
(45) Date of Patent: Mar. 13, 2001

(54) ROTOR STRUCTURE

(75) Inventors: Kyoko Higashino; Yoshihito Asao; Kenji Tsuruhara; Atsushi Oohashi, all of Tokyo (JP)

(73) Assignee: Mitsubishi Denki Kabushiki Kaisha, Tokyo (JP)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: 09/531,223

(22) Filed: Mar. 20, 2000

(30) Foreign Application Priority Data

Sep. 17, 1999 (JP) 11-264130

(51) Int. Cl.⁷ H02K 21/14

(52) U.S. Cl. 310/263; 310/156; 310/261

(58) Field of Search 310/263, 156, 310/257, 192, 261

(56) References Cited

U.S. PATENT DOCUMENTS

5,306,977 * 4/1994 Hayashi et al. 310/263

5,483,116 * 1/1996 Kusase et al. 310/263

5,747,913 * 5/1998 Amlee et al. 310/263
5,903,084 * 5/1999 Asao et al. 310/263

FOREIGN PATENT DOCUMENTS

11-136913 5/1999 (JP) H02K/19/22

* cited by examiner

Primary Examiner—Burton Mullins

(74) Attorney, Agent, or Firm—Sughrue, Mion, Zinn, Macpeak & Seas, PLLC

(57)

ABSTRACT

A rotor structure comprising a rotor coil for generating a magnetic flux, a pole core which covers the rotor coil and consists of a first pole core body and a second pole core body, each having a plurality of claw-like magnetic poles which are mated with each other, magnets provided on both sides of each of the claw-like magnetic pole for suppressing the leakage of a magnetic flux between adjacent claw-like magnetic poles, and reinforcements for holding the magnets in such a manner that the magnets are inclined so that the interval between the magnets becomes larger on the outer side than on the inner side.

This rotor structure can reduce centrifugal force applied to the magnets.

20 Claims, 14 Drawing Sheets

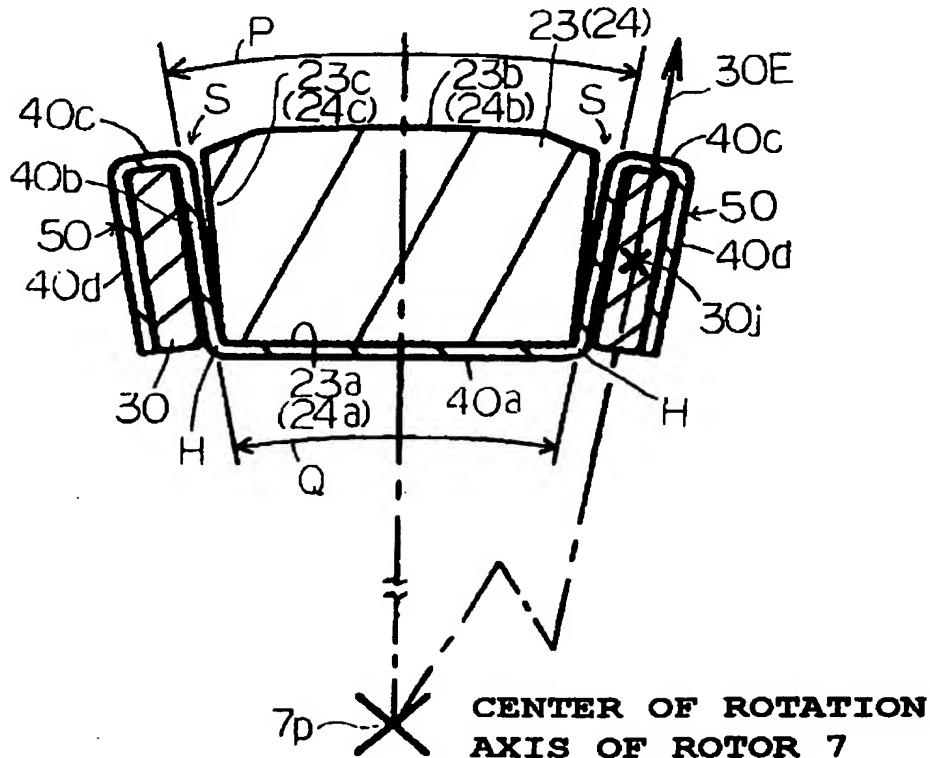


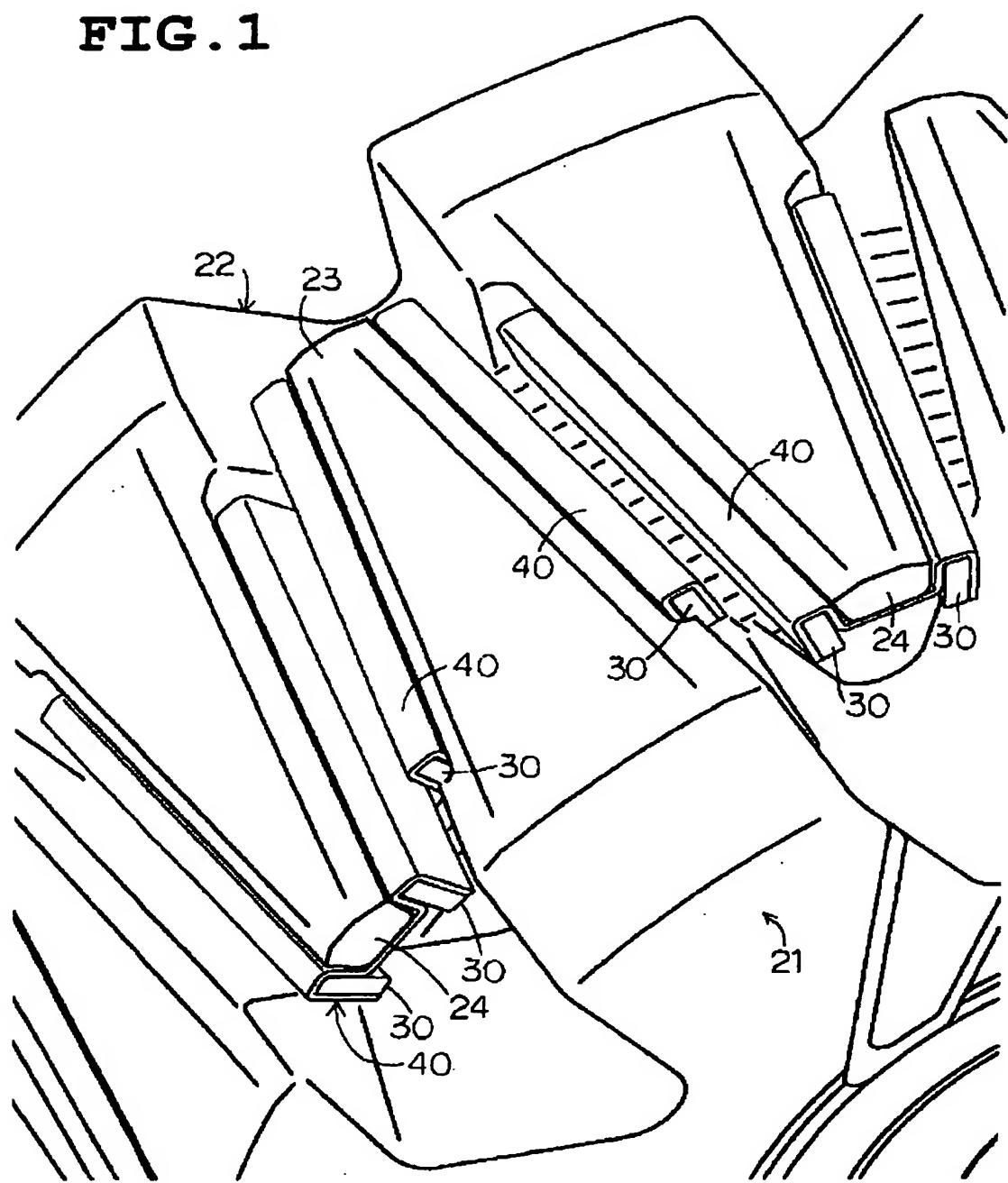
FIG. 1

FIG. 2

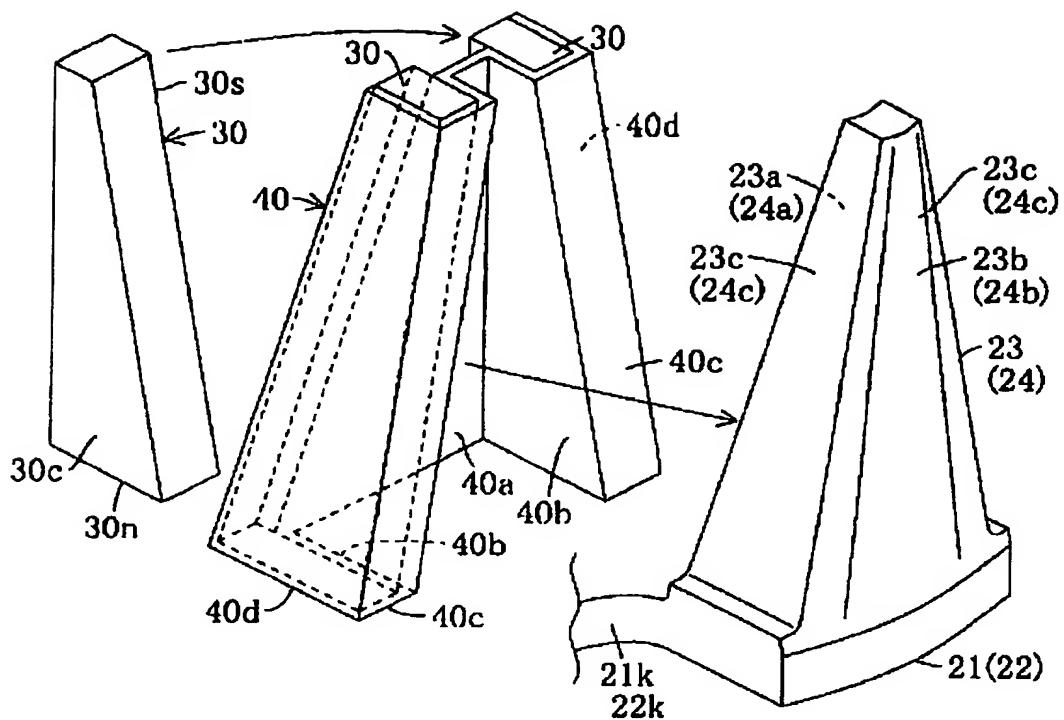


FIG. 3

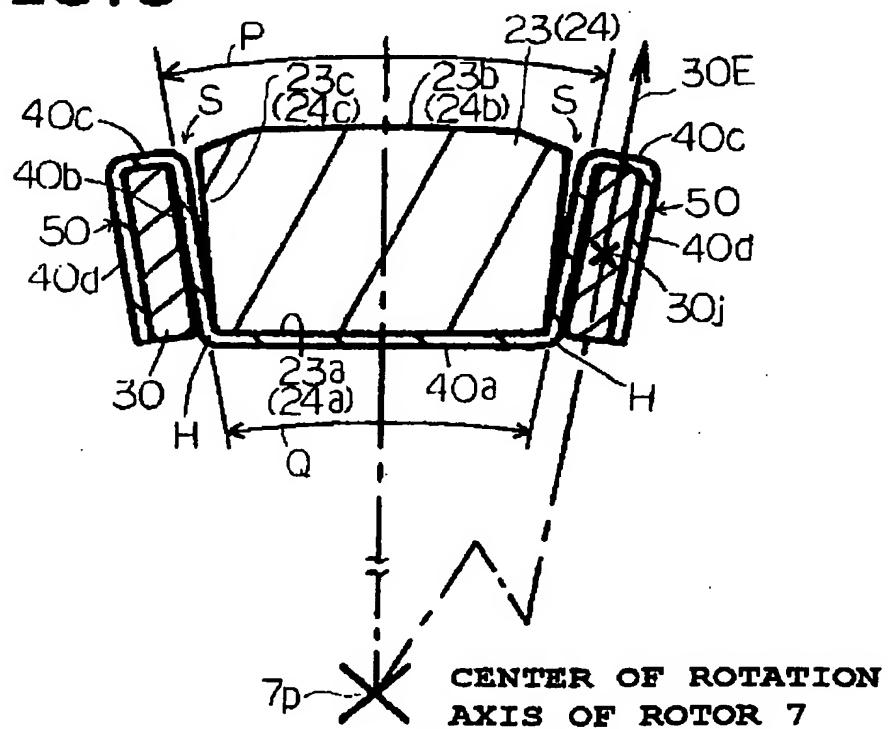


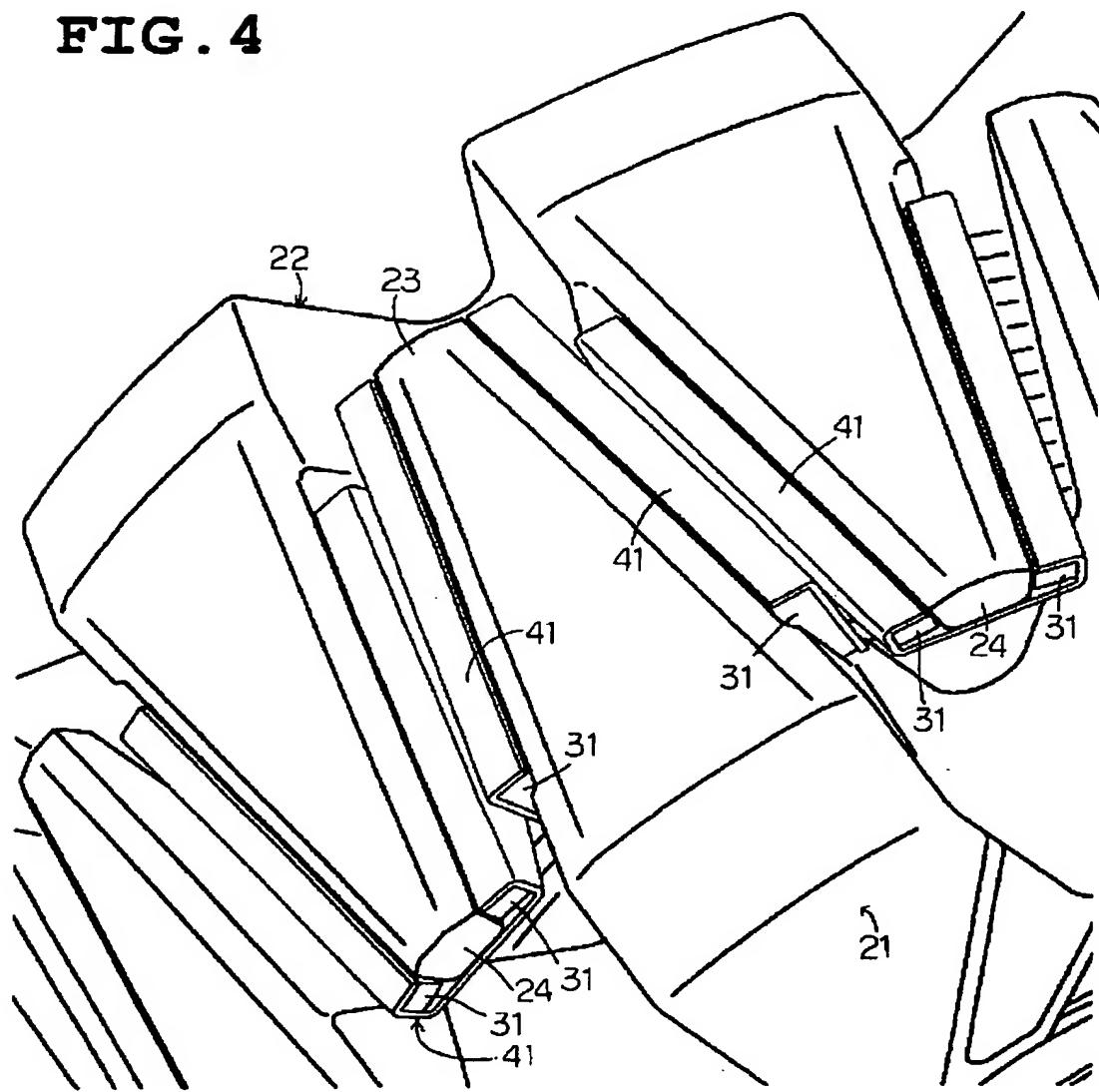
FIG. 4

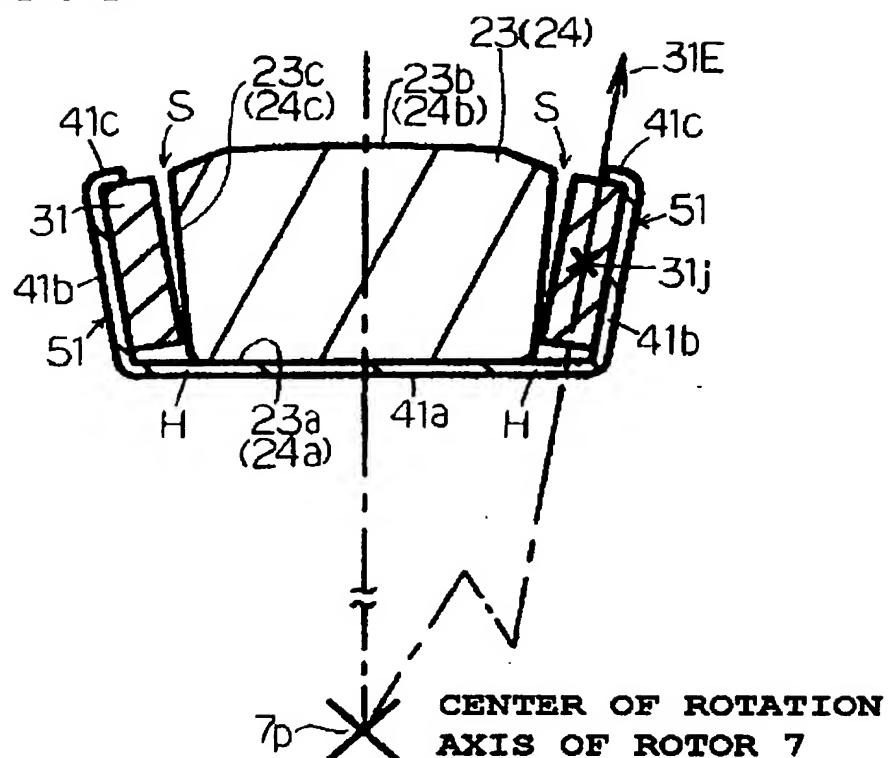
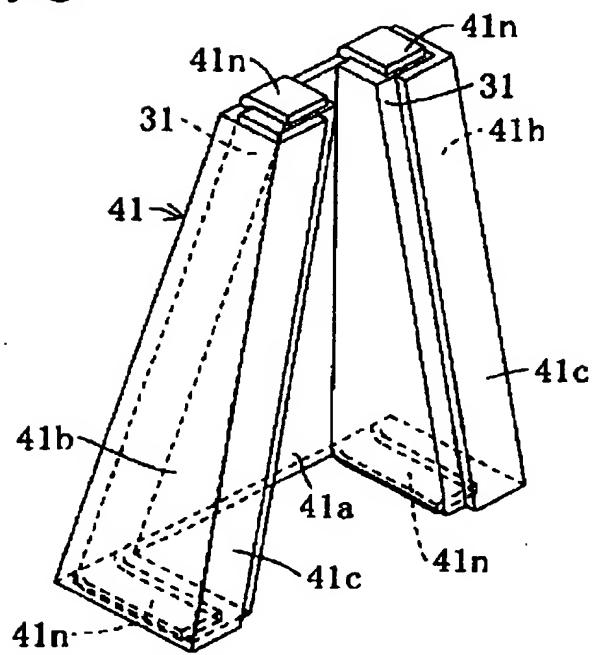
FIG. 5**FIG. 6**

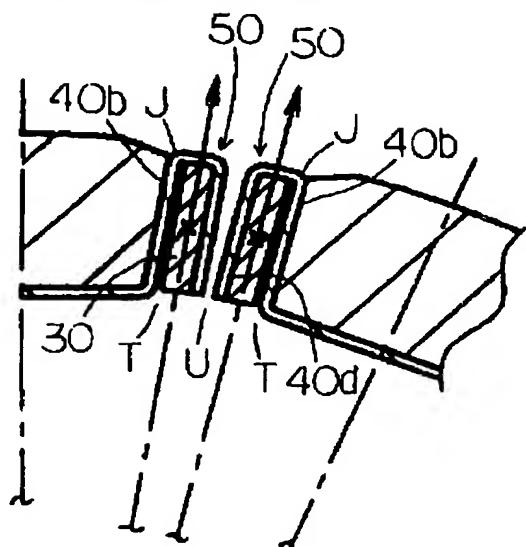
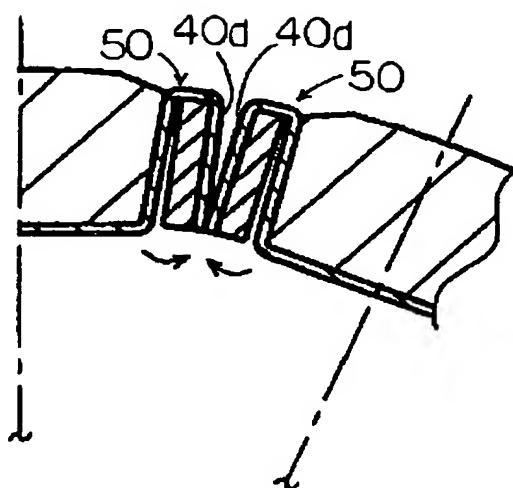
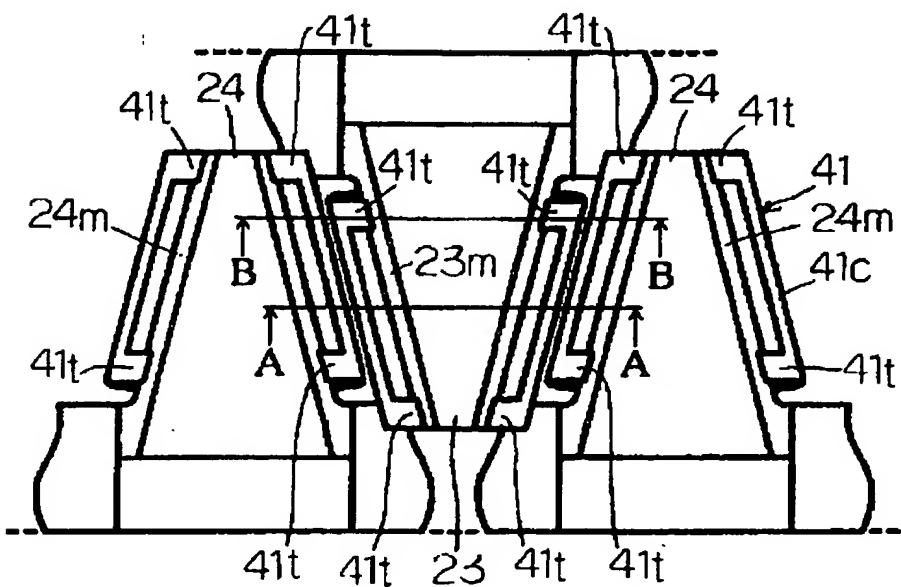
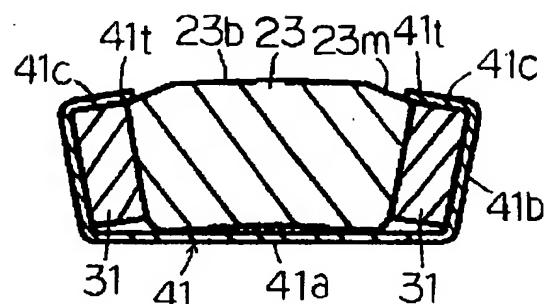
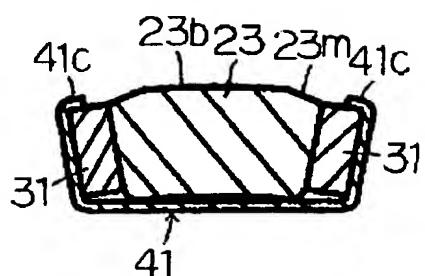
FIG. 7 (a)**FIG. 7 (b)**CENTER OF ROTATION
AXIS OF ROTOR 7CENTER OF ROTATION
AXIS OF ROTOR 7**FIG. 8**

FIG. 9 (a)



B-B CROSS SECTION

FIG. 9 (b)



A-A CROSS SECTION

FIG. 10

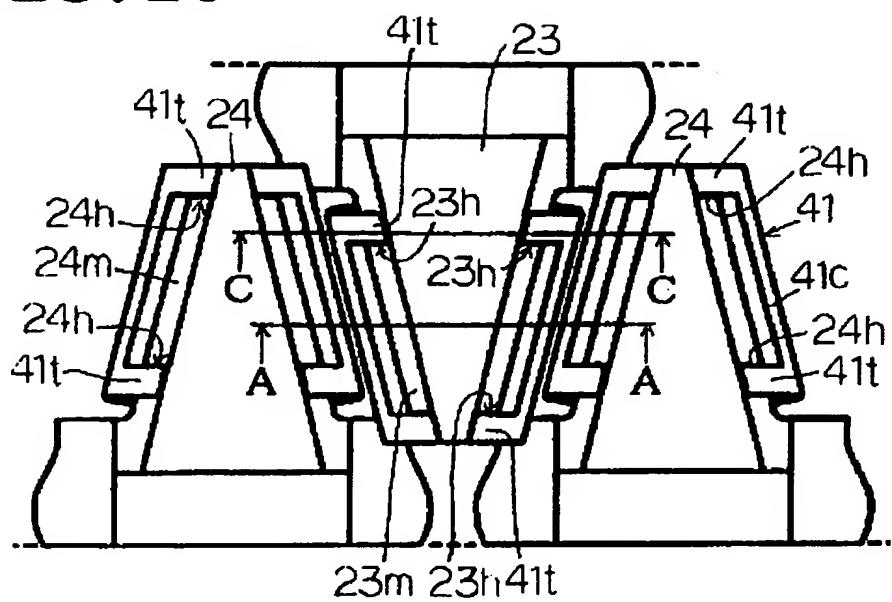


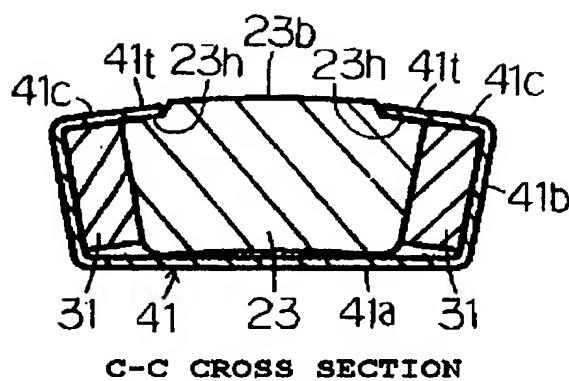
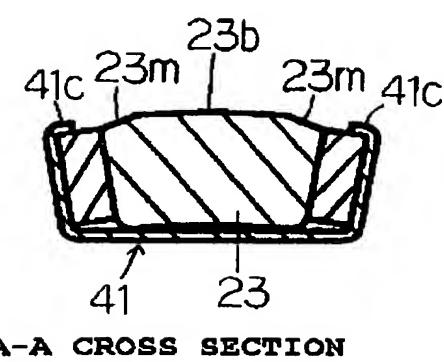
FIG. 11(a)**FIG. 11(b)**

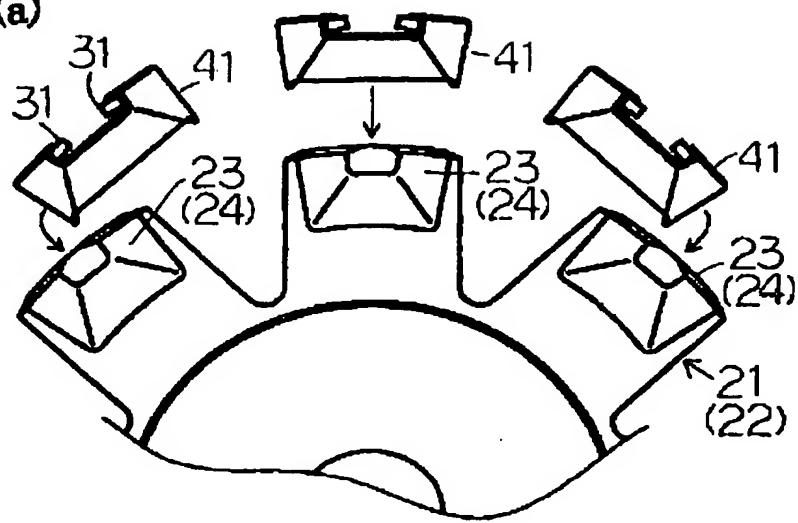
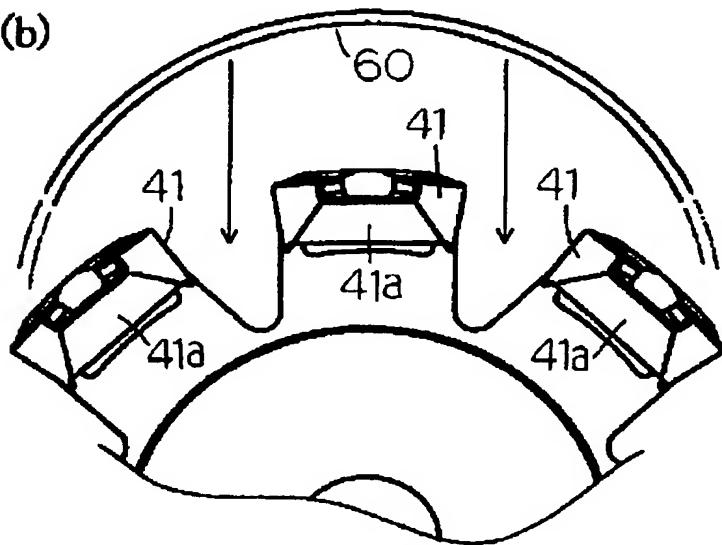
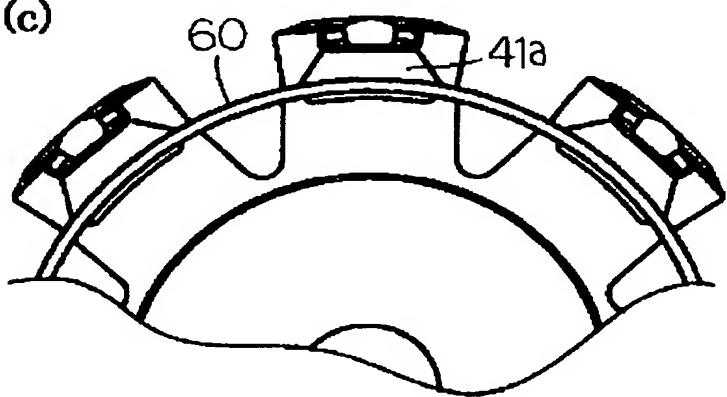
FIG. 12 (a)**FIG. 12 (b)****FIG. 12 (c)**

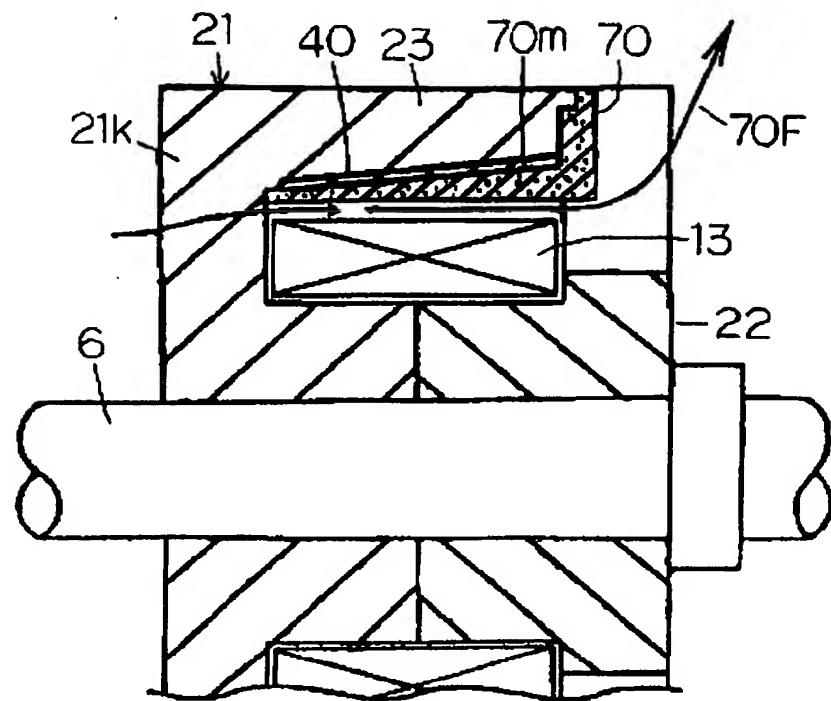
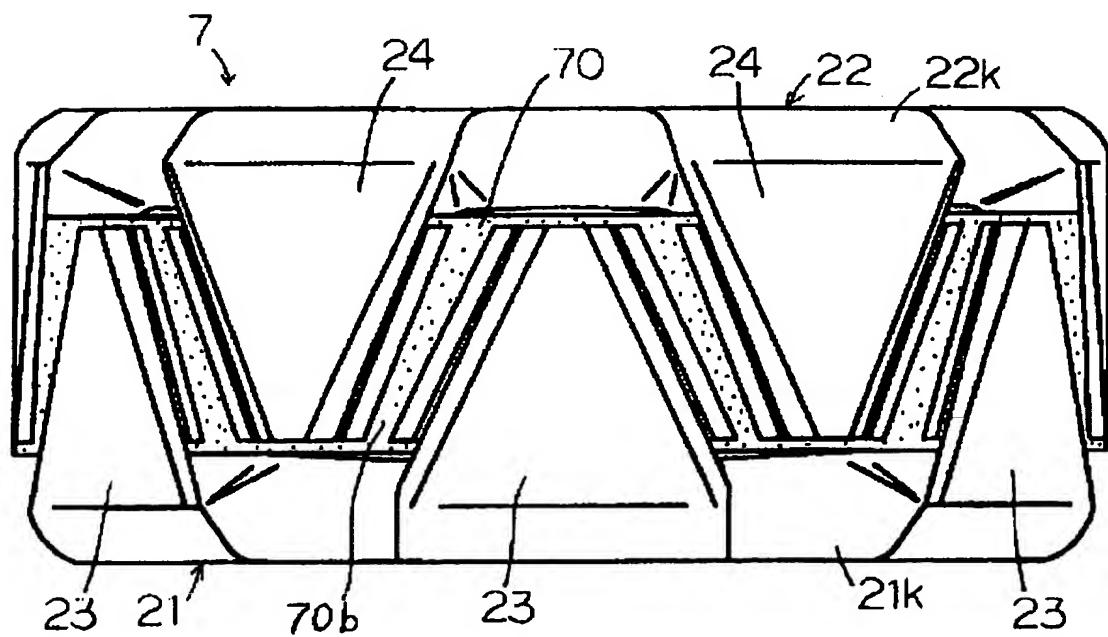
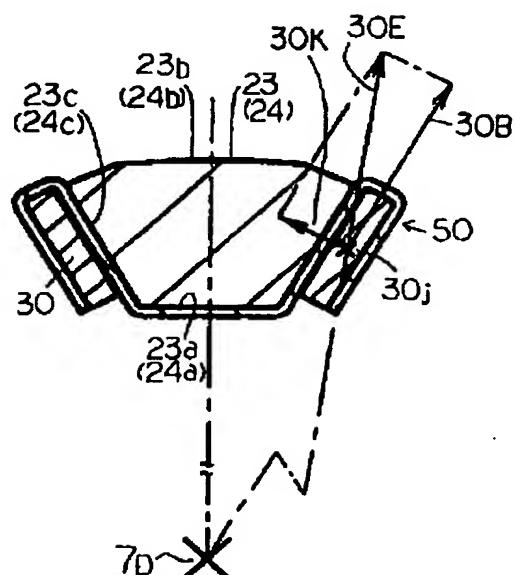
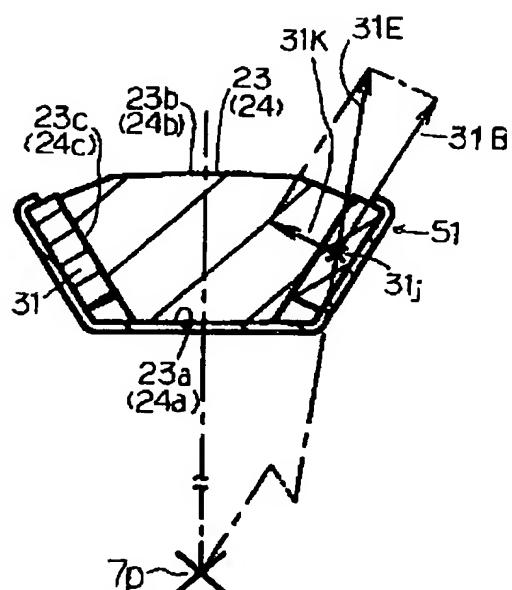
FIG. 13**FIG. 14**

FIG. 15(a)

CENTER OF ROTATION
AXIS OF ROTOR 7

FIG. 15 (b)

CENTER OF ROTATION
AXIS OF ROTOR 7

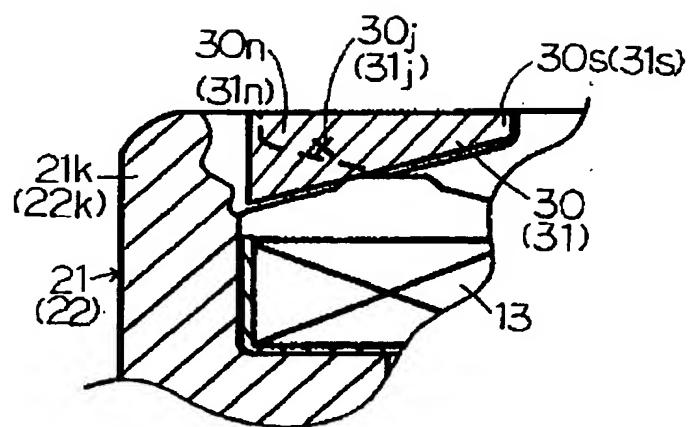
FIG. 16

FIG. 17 PRIOR ART

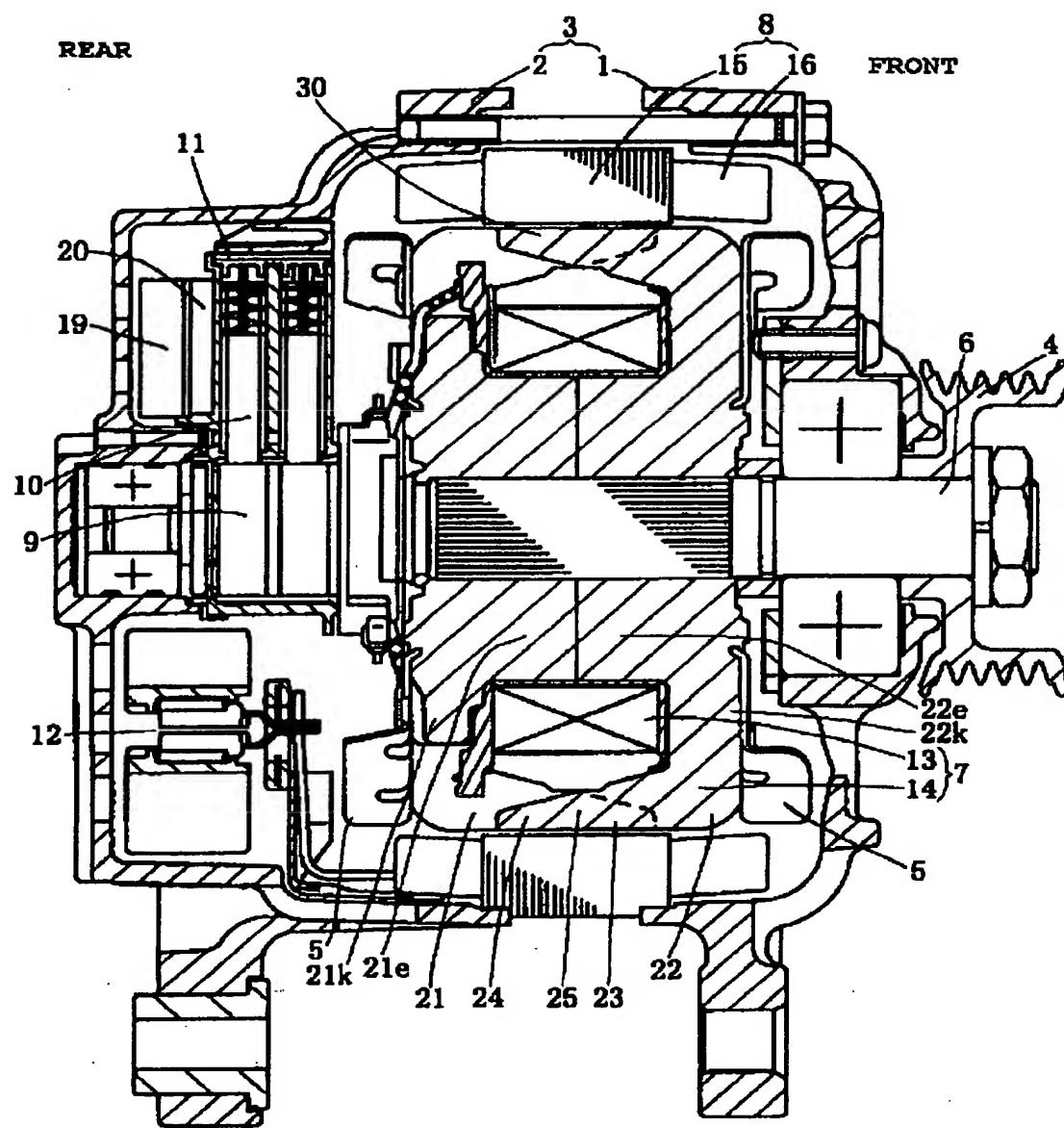


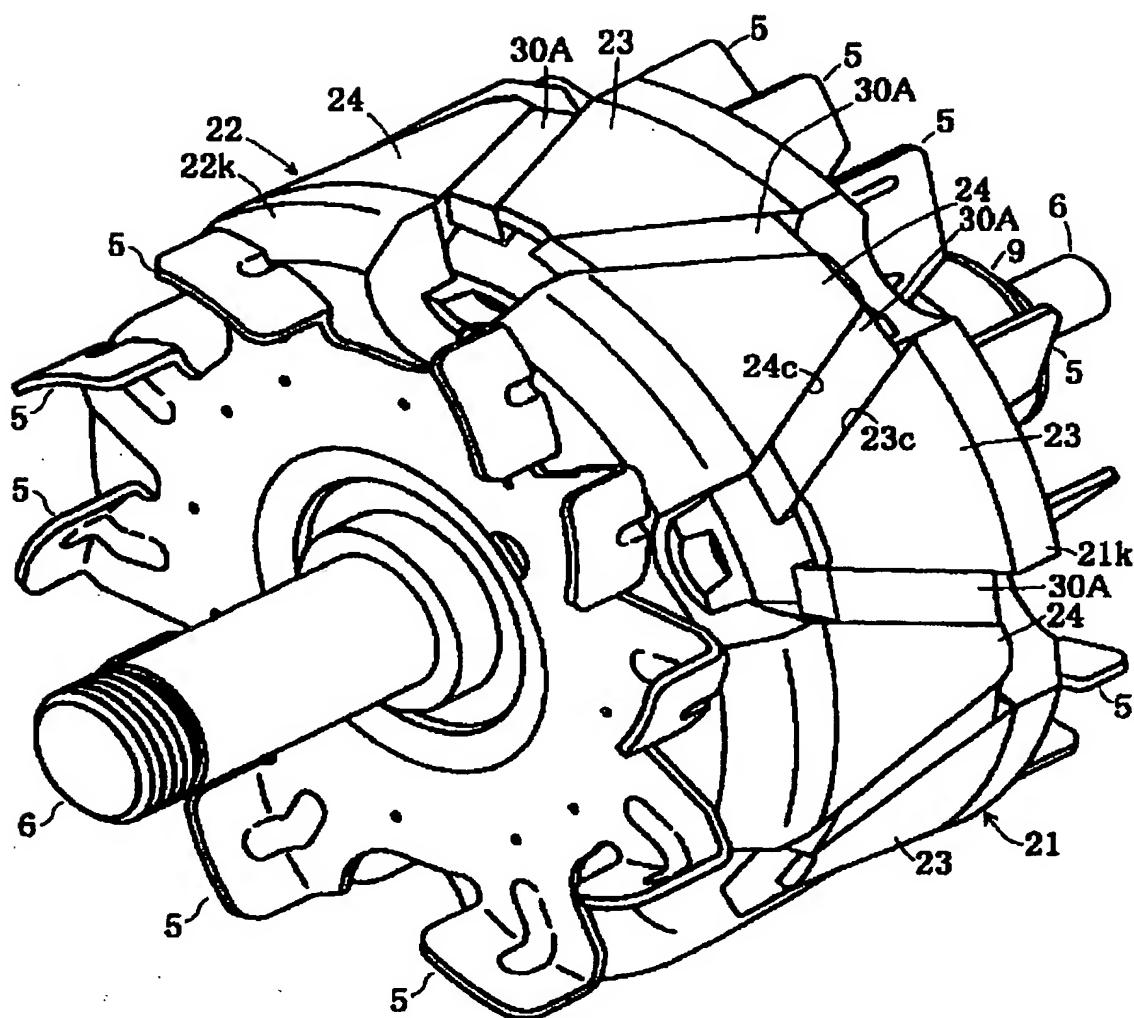
FIG. 18 PRIOR ART

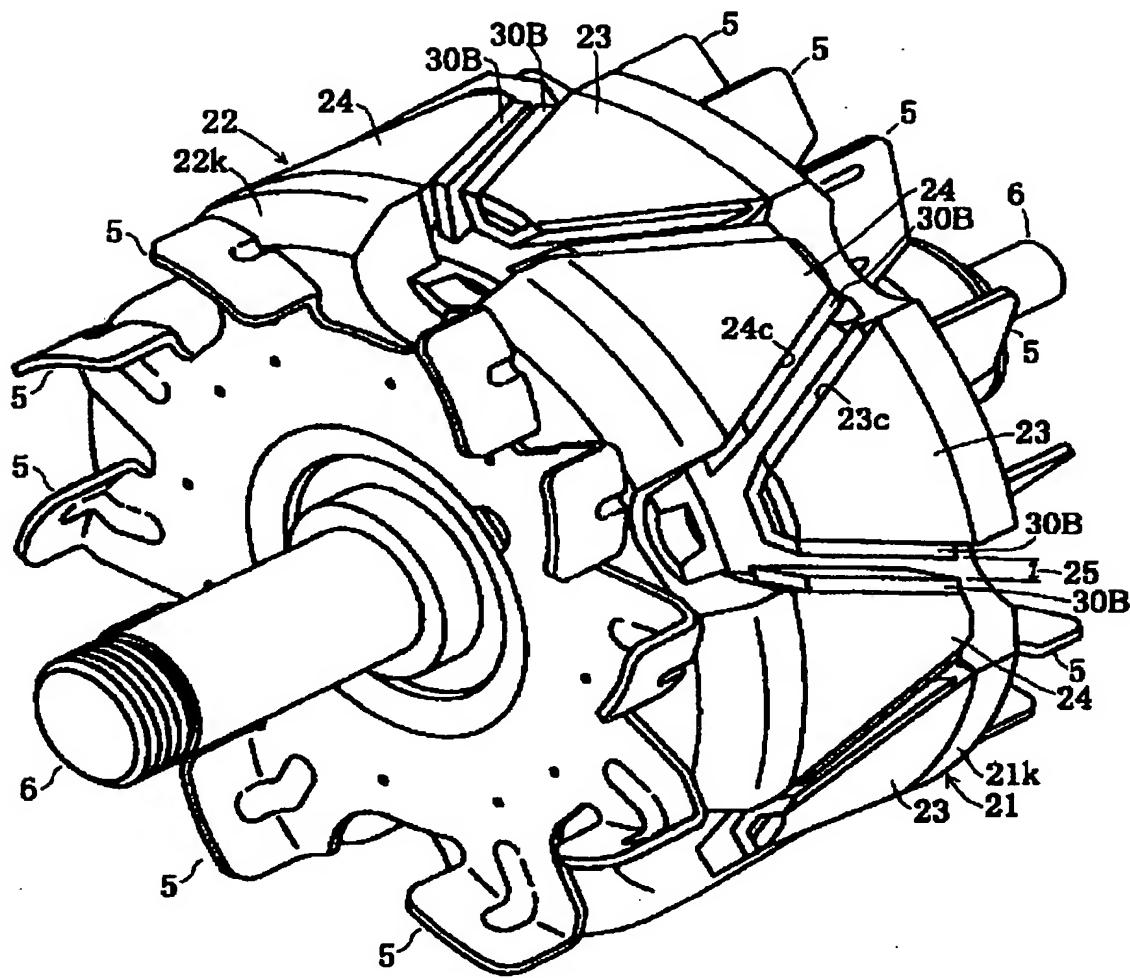
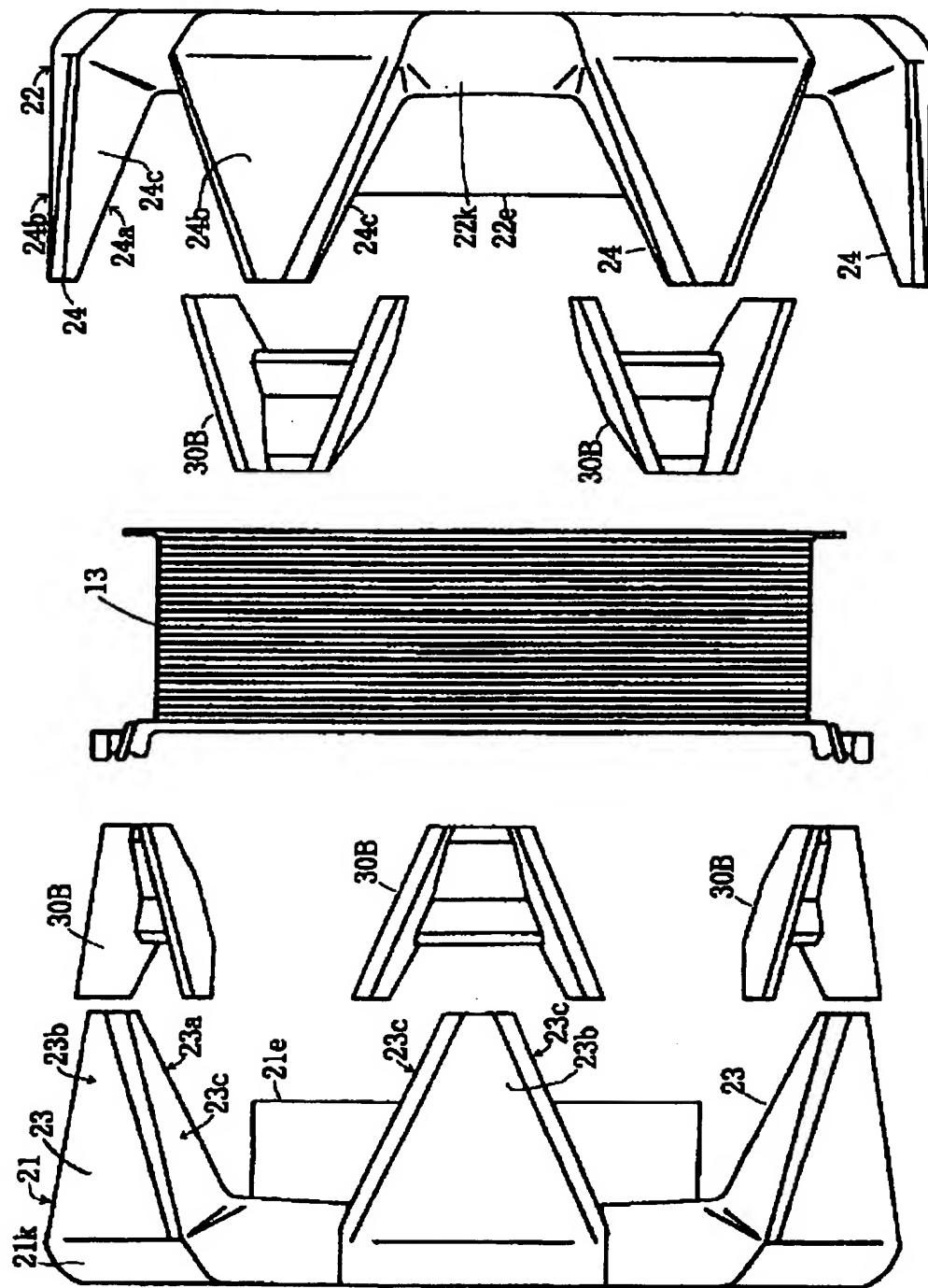
FIG. 19 PRIOR ART

FIG. 20 PRIOR ART



ROTOR STRUCTURE

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a rotor structure for an AC generator or a motor and, particularly, to a structure for attaching magnets for preventing the leakage of a magnetic flux between claw-like magnetic poles.

2. Description of the Prior Art

FIG. 17 is a sectional side view of a prior art rotor structure for an AC generator or a motor, FIG. 18 is a perspective view of the rotor, and FIG. 20 is an exploded side view of individual parts of the rotor.

As shown in FIG. 17, this generator comprises a case 3 consisting of an aluminum front bracket 1 and an aluminum rear bracket 2, a shaft 6 which is installed in the case 2 and one end of which is fitted with a pulley 4, a Randle type rotor 7 fixed to the shaft 6, fans 5 fixed to both end surfaces of the rotor 7, a stator 8 fixed to the inner wall of the case 3, slip rings 9 which are fixed to the other end of the shaft 6 and supply a current to the rotor 7, a pair of brushes 10 in sliding contact with the slip rings 9, a brush holder 11 for storing the brushes 10, a rectifier 12 which is electrically connected to the stator 8 and rectifies an alternating current generated in the stator 8 into a direct current, a heat sink 19 attached to the brush holder 11, and a regulator 20 which is attached to the heat sink 19 and regulates an AC voltage generated in the stator 8.

The rotor 7 comprises a cylindrical rotor coil 13 for generating a magnetic flux with a current and a pole core 14 which covers the rotor coil 13 and forms a magnetic pole with the magnetic flux of the rotor coil 13.

The stator 8 comprises a stator core 15 and a stator coil 16 which is wound round the stator core 15 and generates an alternating current by a change in magnetic flux from the rotor coil 13 caused by the rotation of the rotor 7.

The pole core 14 consists of a first pole core body 21 and a second pole core body 22 which are mated with each other.

The pole core body 21 and the pole core body 22 are generally made from iron and consist of cylindrical portions 21e and 22e wound with the rotor coil 13 and disk-like base portions 21k and 22k from which the cylindrical portions 21e and 22e project, respectively. The base portions 21k and 22k have at the peripheries a plurality of claw-like magnetic poles 23 and 24 which are mated with each other between the outer wall of the rotor coil 13 and the inner wall of the stator 8, respectively.

The thickness and width of each of the claw-like magnetic poles 23 and 24 are large on the base portion 21k and 22k sides and become smaller toward the end sides.

The inner faces 23a and 24a of the claw-like magnetic poles 23 and 24 become thinner toward the ends and the outer faces 23b and 24b are arched in conformity with the inner wall of the stator 8. Each of the claw-like magnetic poles 23 and 24 has two trapezoidal side faces 23c and 24c in a circumferential direction of the rotor 7. Since each pair of claw-like magnetic poles 23 and 24 are mated with each other, the inner faces 23a and 24a of the claw-like magnetic poles 23 and 24 are arranged alternately in a circumferential direction. The side faces 23c and 24c of the claw-like magnetic poles 23 and 24 are inclined toward the centers of the claw-like magnetic poles 23 and 24 so that they become thinner from the root side toward the end side.

As shown in FIG. 18, a rectangular magnet 30A magnetized to suppress the leakage of a magnetic flux between the

opposed side faces 23c and 24c is fixed between the adjacent claw-like magnetic poles 23 and 24.

A description is subsequently given of the operation of the generator. A current is supplied from an unshown battery to the rotor coil 13 through the brushes 10 and the slip rings 9 to generate a magnetic flux, whereby the claw-like magnetic poles 23 of the first pole core body 21 are magnetized to an N pole and the claw-like magnetic poles 24 of the second pole core body 22 are magnetized to an S pole. Meanwhile, the pulley 4 is turned by the rotation force of an engine and the rotor 7 is turned by the shaft 6, thereby generating electromotive force in the stator coil 16. This AC electromotive force is rectified into a direct current by the rectifier 12, regulated by the regulator 20 and charged into the unshown battery.

15 The above magnet 30A which is inserted between the claw-like magnetic poles 23 and 24 and is rectangular or may be various in shape, for example, ring-shaped or ring-shaped and packed in other resin is fixed to the claw-like magnetic poles 23 and 24 by fixing means.

20 However, the following problems may occur. That is, since stress is applied to the magnet 30A at the time of production or centrifugal force generated by rotation is applied to the magnet 30A, the magnet 30A is inferior in durability.

25 Further, since the pole core bodies 21 and 22 are generally produced by forging, details of the claw-like magnetic poles 23 and 24 which have a specially complex shape cannot have high accuracy. There are differences in size between the claw-like magnetic poles 23 and 24. It is difficult to manufacture the magnet 30A which is formed in conformity with the inner faces 23a and 24a of the claw-like magnetic poles 23 and 24 which differ from each other and a support member which is molded in conformity with the claw-like magnetic poles 23 and 24.

30 35 When the magnet 30A is manufactured in consideration of molding ease, it becomes fragile. Therefore, when it is installed near the claw-like magnetic poles 23 and 24 of the rotor 7, some measure is necessary. However, when the magnet 30A is made sufficiently thick or very strong, it costs dear, making it difficult to mass-produce it.

40 Suppose that the magnet 30A and the support member are produced in accordance with the differences and that differences in the gaps between the claw-like magnetic poles 23 and 24 and the magnet 30A and between the claw-like magnetic poles 23 and 24 and the support member are made small. Even if the differences are small, when the magnet 30A receives centrifugal force at the time of the rotation of the rotor 7, a great force difference is produced, thereby making it possible that the magnet 30A and the support member are damaged.

45 50 When the magnet 30A is supported by the side faces 23C and 24C of the claw-like magnetic poles 23 and 24 irrespective of the inner faces 23a and 24a of the claw-like magnetic poles 23 and 24, force may be applied to the magnet 30A by the dislocation of each of the two pole core bodies 21 and 22 when they are mated with each other or dislocation caused by rotation force.

55 60 The end portions of the claw-like magnetic poles 23 and 24 are moved toward the rotor coil 13 and the stator 8 by centrifugal force generated by the rotation of the rotor 7 and the magnetic attraction force of the stator 8 at the time of power generation. Thereby, a load is applied to the magnet 30A between the claw-like magnetic poles 23 and 24, whereby the magnet 30A may be distorted or broken.

65 A countermeasure against this is disclosed by Japanese Laid-open Patent Application No. 11-136913. In this

publication, a magnet 30B is formed as shown in FIG. 19 and FIG. 20. That is, the magnet 30B is fixed to each of the claw-like magnetic poles 23 and 24 in such a manner that it covers the inner face 23a or 24a and the side faces 23c or 24c of the claw-like magnetic pole 23 or 24. A space 25 is formed between adjacent magnets 30B. Thereby, a set of the claw-like magnetic pole 23 and the magnet 30B and a set of the claw-like magnetic pole 24 and the magnet 30B move independently, thereby preventing the application of a load to the magnet 30B and the breakage of the magnet 30B.

SUMMARY OF THE INVENTION

However, the invention disclosed by Japanese Laid-open Patent Application No. 11-136913 is not aimed to reduce the influence of centrifugal force generated by the rotation of the rotor 7 upon the magnet 30B.

That is, since the magnet 30B which moves together with the claw-like magnetic poles 23 and 24 is more fragile than the claw-like magnetic poles 23 and 24, the magnet 30B has low durability against centrifugal force. Further, since the magnet 30B is completely exposed, it is conceivable that it may be damaged by a suspending substance contained in the case 3. Further, as the magnet 30B is fixed to the claw-like magnetic poles 23 and 24 by the uneven surface of the magnet 30B, it is unsatisfactory in terms of strength against rotation.

A support member such as a tape is wound round each of the claw-like magnetic poles 23 and 24 to absorb centrifugal force applied to the magnet 30B. This does not take into consideration the movement of the magnet 30B during rotation and hence, the magnet 30B cannot be always held properly by the tape. That is, the weight of the support member is applied to the magnet 30B by the rotation of the rotor 7, or the magnet 30B is supported nonuniformly, whereby not only the magnet 30B but also the support member may be broken at the time of high-speed rotation.

When the side faces 23c and 24c of the claw-like magnetic poles 23 and 24 are inclined in an axial direction or in a radial direction, the magnet 30B fixed to the claw-like magnetic poles 23 and 24 is also inclined. When the magnet 30B is to be fixed, it may be inclined toward the center of the axis or get out of place. Therefore, the magnet 30B must be temporarily positioned to prevent this, thereby taking time and labor to fix. When the two pole core bodies 21 and 22 are to be mated with each other in such a manner that they surround the rotor coil 13, the magnets 30B for either one of the claw-like magnetic poles 23 and 24 are inclined and dropped. Further, when the shaft 6 is installed in the case and the generator is carried, there is a possibility that the magnets 30B may fall off toward the center of the axis.

When an adhesive is applied to the magnets 30 in order to temporarily fix the magnets 30 to the claw-like magnetic poles 23 and 24 at this point, it is known that it is good to apply force for bringing adhesion surfaces close to each other in order to secure the positional relationship between them before drying and fixing. In this respect, force is readily applied to the above claw-like magnetic poles 23 and 24 and the above magnets 30 in such a direction that they are separated from each other, and a holding step is further required in the step of coating an adhesive, thereby making it possible that the assembly work becomes very complicated and cost becomes high. If some trouble occurs during this, when a rotor structure is used as a car AC generator which is used in a severe environment such as high temperatures or low temperatures for a long time, bonding portions between the claw-like magnetic poles 23 and 24

and the magnets 30B may deteriorate with the result that the magnets 30 may be scattered.

It is an object of the present invention which has been made to solve the above problems to reduce centrifugal force applied to magnets for suppressing the leakage of a magnetic flux between claw-like magnetic poles at the time of rotation of the rotor and to attach the magnets to the claw-like magnetic poles.

According to a first aspect of the present invention, there is provided a rotor structure comprising a rotor coil for generating a magnetic flux, a pole core which covers the rotor coil and consists of a first pole core body and a second pole core body, each having a plurality of claw-like magnetic poles which are mated with each other, magnets provided on both sides of each claw-like magnetic pole to suppress the leakage of a magnetic flux between the side faces of adjacent claw-like magnetic poles, and reinforcements for holding the magnets in such a manner that the magnets are inclined so that the interval between the magnets becomes larger on the outer side than on the inner side.

According to a second aspect of the present invention, there is provided a rotor structure, wherein the reinforcement consists of an inner portion conformed to the inner face of the claw-like magnetic pole, bent portions bent from both ends of the inner portion toward the side faces of the claw-like magnetic pole, pressing portions, bent from the bent portions, for pressing the outer faces of the magnets, and folded portions folded from the pressing portions toward the side faces of the magnets, and the magnets are held on the inner side of the reinforcement.

According to a third aspect of the present invention, there is provided a rotor structure, wherein the reinforcement consists of an inner portion conformed to the inner face of the claw-like magnetic pole and the inner faces of the magnets, bent portions bent from both ends of the inner portion toward the side faces of the magnets, and pressing portions, projecting from the bent portions toward the claw-like magnetic pole, for pressing the outer faces of the magnets, and the magnets are held on the outer side of the reinforcement.

According to a fourth aspect of the present invention, there is provided a rotor structure, wherein the magnet and portions holding the magnet of the reinforcement constitute a side magnet body, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, the side magnet body moves toward the claw-like magnetic pole to reduce the space when centrifugal force is applied to the magnet, and the reinforcement is deformed by this moving force to absorb the centrifugal force.

According to a fifth aspect of the present invention, there is provided a rotor structure, wherein the center of the movement of the side magnet body is located on the claw-like magnetic pole side of a line connecting the center of the rotation axis of the rotor and the gravity center of the magnet, and the movement of the side magnet body is stopped when it contacts the side face of the claw-like magnetic pole.

According to a sixth aspect of the present invention, there is provided a rotor structure, wherein the magnet is held by the pressing portion and the folded portion and constitutes a side magnet body together with the pressing portion and the folded portion, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, a space is formed between adjacent side magnet bodies, the side magnet body moves toward the adjacent side magnetic body to reduce the space between the adjacent side magnet

bodies when centrifugal force is applied to the magnet, the reinforcement is deformed by this moving force to absorb the centrifugal force, and the movement of the side magnet body is stopped when the adjacent folded portions contact each other.

According to a seventh aspect of the present invention, there is provided a rotor structure, wherein the space between the side magnet body and the side face of the claw-like magnetic pole is set such that the deformed reinforcement can restore its original shape when centrifugal force is not applied to the magnet after the movement of the side magnet body is stopped and the deformation amount of the reinforcement becomes maximum.

According to an eighth aspect of the present invention, there is provided a rotor structure, wherein the space between the side magnet body and the side face of the claw-like magnetic pole is set such that stress applied to the reinforcement falls below at least an allowable level when the movement of the side magnet body is stopped and the deformation amount of the reinforcement becomes maximum.

According to a ninth aspect of the present invention, there is provided a rotor structure, wherein an elastic material is placed in the space between the side magnet body and the side face of the claw-like magnetic pole.

According to a tenth aspect of the present invention, there is provided a rotor structure which has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in an inward direction.

According to an eleventh aspect of the present invention, there is provided a rotor structure which has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in an outward direction.

According to a twelfth aspect of the present invention, there is provided a rotor structure which has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in inward and outward directions.

According to a thirteenth aspect of the present invention, there is provided a rotor structure, wherein the above stopping structure is contacting portions which project from the reinforcement and contact the outer face of the claw-like magnetic pole.

According to a fourteenth aspect of the present invention, there is provided a rotor structure, wherein a pressing member for pressing the reinforcements against the claw-like magnetic poles from the inner side is used as the stopping structure.

According to a fifteenth aspect of the present invention, there is provided a rotor structure, wherein the pressing member has a cylindrical peripheral surface, grooves in which the claw-like magnetic poles held in the reinforcements are fitted in are formed in the peripheral surface, and the outer faces of the claw-like magnetic poles and the peripheral surface of the pressing member form the cylindrical curved peripheral surface of the rotor.

According to a sixteenth aspect of the present invention, there is provided a rotor structure, wherein the side faces of the claw-like magnetic pole are inclined such that the interval between them becomes larger on the outer side than on the inner side.

According to a seventeenth aspect of the present invention, there is provided a rotor structure, wherein the gravity center of the magnet is located close to the root side of the claw-like magnetic pole.

According to an eighteenth aspect of the present invention, there is provided a rotor structure, wherein the reinforcement is made from a metal.

According to a nineteenth aspect of the present invention, there is provided a rotor structure, wherein the reinforcement is welded to the claw-like magnetic pole.

According to a twentieth aspect of the present invention, there is provided a rotor structure, wherein the reinforcement has a stopping structure for preventing the magnets from falling off toward the end side or root side of the reinforcement.

The above and other objects, features and advantages of the invention will become more apparent from the following description when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE ACCOMPANYING DRAWINGS

FIG. 1 is a perspective view of key parts of a rotor structure according to Embodiment 1 of the present invention;

FIG. 2 is an exploded perspective view of the key parts of the rotor structure according to Embodiment 1;

FIG. 3 is a sectional view in an axial direction of a claw-like magnetic pole, a reinforcement and magnets according to Embodiment 1;

FIG. 4 is a perspective view of key parts of a rotor structure according to Embodiment 2;

FIG. 5 is a sectional view in an axial direction of a claw-like magnetic pole, a reinforcement and magnets according to Embodiment 2;

FIG. 6 is a perspective view of the stopping portions of the reinforcement according to Embodiment 2;

FIGS. 7(a) and 7(b) are sectional views in an axial direction of a claw-like magnetic pole, a reinforcement and magnets according to Embodiment 3;

FIG. 8 is a schematic side view of contacting portions according to Embodiment 4;

FIGS. 9(a) and 9(b) are sectional views in an axial direction of a claw-like magnetic pole and contacting portions of a reinforcement and magnets according to Embodiment 4;

FIG. 10 is a schematic side view of stepped portions according to Embodiment 5;

FIGS. 11(a) and 11(b) are sectional views in an axial direction of stepped portions of a claw-like magnetic pole, contacting portions of a reinforcement and magnets according to Embodiment 5;

FIGS. 12(a), 12(b) and 12(c) are plan views of a pressing member set on reinforcements according to Embodiment 6;

FIG. 13 is a sectional view in an axial direction of a pressing member according to Embodiment 7;

FIG. 14 is a side view of a pressing member and a rotor according to Embodiment 7;

FIGS. 15(a) and 15(b) are sectional views in an axial direction of the side faces of a claw-like magnetic pole, a reinforcement and magnets according to Embodiment 8;

FIG. 16 is a sectional view in a circumferential direction of a claw-like magnetic pole and magnets according to Embodiment 9;

FIG. 17 is a sectional view of a car AC generator for explaining a prior art rotor structure;

FIG. 18 is a perspective view for explaining a prior art rotor structure;

FIG. 19 is a perspective view for explaining a prior art rotor structure; and

FIG. 20 is an exploded side view for explaining a prior art rotor structure.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Preferred embodiments of the present invention will be described herein under with reference to the accompanying drawings.

Embodiment 1

FIGS. 1 to 3 show a rotor structure for use in a car AC generator according to Embodiment 1 of the present invention. FIG. 1 is a perspective view of key parts of a rotor for a car AC generator, FIG. 2 is an exploded perspective view and FIG. 3 is a sectional view of a reinforcement. The same and corresponding elements as those of FIGS. 17 to 20 are given the same reference symbols.

As shown in FIG. 1, a ferrite magnet 30 magnetized to suppress the leakage of a magnetic flux between claw-like magnetic poles 23 and 24 is provided on both side faces 23c and 23c of each claw-like magnetic pole 23 and both side faces 24c and 24c of each claw-like magnetic pole 24.

The magnets 30 are held to the claw-like magnetic pole 23 or 24 by a reinforcement 40 which is deformed to absorb centrifugal force applied to the magnets 30 at the time of rotation of a rotor 7 in such a manner they are inclined so that the interval between the magnets 30 becomes larger on the outer side than on the inner side. The reinforcement 40 is made of a metal plate such as a stainless steel plate having a thickness of about 0.5 mm and easily manufactured by bending a single metal plate by pressing.

As shown in FIG. 2 and FIG. 3, this reinforcement 40 has a substantially M-shaped cross section in an axial direction of the rotor 7 and consists of a trapezoidal inner portion 40a conformed to the inner face 23a or 24a of the claw-like magnetic pole 23 or 24, bent portions 40b bent outward from both ends of the inner portion 40a and conformed to both side faces 23c or 24c of the claw-like magnetic pole 23 or 24, pressing portions 40c bent from the ends of the bent portions 40b toward the outer faces of the magnets 30 and pressing the outer faces of the magnets 30, and folded portions 40d folded from the pressing portions 40c toward the side faces of the magnets 30.

The magnets 30 are surrounded by the bent portions 40b, the pressing portions 40c and the folded portions 40d and sandwiched between the bent portions 40b and the folded portions 40d to hold them on the inner side of the reinforcement 40 from the outer side.

As shown in FIG. 3, the inner portion 40a and the bent portions 40b and 40b at both ends of the inner portion 40a form an almost U shape in such a manner that the bent portions 40b and 40b are inclined so that the length Q on the inner side becomes smaller than the length P on the outer side. The bent portions 40b, the pressing portions 40c and the folded portions 40d of the reinforcement 40 surrounding the magnets 30 form an inverted U shape in conformity with the cross section of the magnet 40.

That is, the magnets 30 are provided on both side faces 23c or 24c of the claw-like magnetic pole 23 or 24 in such a manner that they are inclined from the center line of the claw-like magnetic pole 23 or 24 passing through the center 7p of the rotation axis of the rotor 7 toward the outer face 23b or 24b.

As shown in FIG. 2, the magnet 30 does not require a holding portion for the claw-like magnetic pole 23 or 24, and the side faces 30c of the magnet are trapezoidal in conformity with the side face 23c or 24c of the claw-like magnetic pole 23 or 24. The magnet 30 is shaped like a headed quadrangular pyramid whose width is almost fixed and thickness increases from the end 30s side toward the root 30n side in conformity with the shape of the claw-like magnetic pole 23 or 24. The magnet 30 may be rectangular.

An adhesive or the like is used to hold the magnet 30 by the reinforcement 40 and fix it to the claw-like magnetic pole 23 or 24. That is, the boundary between the inner portion 40a of the reinforcement 40 and the inner face 23a or 24a of the claw-like magnetic pole 23 or 24 and the boundary between the bent portion 40b, pressing portion 40c and folded portion 40d of the reinforcement 40 and the magnet 30 are coated with an adhesive.

To fix the magnet 30 to the claw-like magnetic pole 23 or 24, the side face 23c or 24c of the claw-like magnetic pole 23 or 24 is separated from the bent portion 40b of the reinforcement 40 with a small space S therebetween.

By this constitution, centrifugal force 30E applied to the gravity center 30j of the magnet 30 at the time of the rotation of the rotor 7 in FIG. 3 becomes moment for moving the magnet 30 and portions holding the magnet 30 of the reinforcement 40 and is absorbed by the reinforcement 40. A set of the magnet 30 and the portions holding the magnet 30 of the reinforcement 40 (bent portion 40b, pressing portion 40c and folded portion 40d) is called "side magnet body 50" and moment applied to the side magnet body 50 will be described with reference to FIG. 3.

That is, the side magnet body 50 is supported only at one side because its fulcrum H is located at each end of the inner portion 40a of the reinforcement 40. That is, the fulcrum H is located on the claw-like magnetic pole 23 or 24 side of a line connecting the center 7p of the rotation axis of the rotor 7 and the gravity center 30j of the magnet 30. Thereby, centrifugal force 30E applied to the magnet 30 is applied to the reinforcement 40 as the above moment. The direction of the above moment applied to the side magnet body 50 is the center direction of the reinforcement 40, that is, the center direction of the claw-like magnetic pole 23 or 24 with the fulcrum H as the center of the movement.

Therefore, the outer side of the side magnet body 50 moves and displaces toward the side face 23c or 24c of the claw-like magnetic pole 23 or 24. Stress is applied to the reinforcement 40 by this displacement but the reinforcement 40 is not broken because the above small space S is formed to reduce the stress to a level below an allowable level. In this case, this small space S is set such that the reinforcement 40 restores its original shape when centrifugal force 30E is not applied to the magnet 30 any more after the displacement of the reinforcement 40.

Thereby, the reinforcement 40 holds the claw-like magnetic pole 23 or 24, thereby increasing its holding strength with the result that the connection of the magnet 40 and the claw-like magnetic pole 23 or 24 is promoted.

When the end portion of the claw-like magnetic pole 23 or 24 is moved inward or outward at the time of the rotation of the rotor 7, it is possible that the end portion of the side magnet body 50 is moved outward by the spring-back of the reinforcement 40. However, the displacement of the side magnet body 50 by the above moment occurs in a direction which offsets the above spring-back, thereby making it possible to eliminate such inconvenience that the magnet 30 and the reinforcement 40 fall off from the claw-like magnetic pole 23 or 24.

Since the inner face 23a or 24a of the claw-like magnetic pole 23 or 24 is in contact with the inner portion 40a of the reinforcement 40, heat transmitted to the claw-like magnetic poles 23 and 24 at the time of power generation is radiated by the reinforcement 40. However, the main purpose of Embodiment 1 is to reduce centrifugal force 30E applied to the magnet 30.

The inner face facing the rotor coil 13 of the magnet 30 held by the reinforcement 40 is exposed so that heat generated at the time of power generation is radiated therefrom. Since the remaining three faces of the magnet 30 are almost surrounded by the reinforcement 40, the magnet 30 has high resistance to centrifugal force. Even if a suspending substance should hit the magnet 30 from the outer side, as the magnet 30 is covered with the reinforcement 40, it is not damaged.

The magnet 30 is not chipped at the time of assembly because it is attached to the claw-like magnetic pole 23 or 24 while it is covered with the reinforcement 40 and has no faces in contact with the claw-like magnetic pole 23 or 24.

Although a cut-away portion in which the reinforcement 40 is fitted is formed in the side faces 23c and 24c of the claw-like magnetic poles 23 and 24, the claw-like magnetic poles 23 and 24 are the same as those of the prior art in that they are tapered off toward the ends. Therefore, a space formed between the side faces 23c and 24c of the claw-like magnetic poles 23 and 24 is substantially rhomboid when seen from a circumferential direction. A space formed between the reinforcements 40 by which the magnets 30 are fixed to the side faces 23c or 24c of the claw-like magnetic poles 23 and 24 is narrow in width but substantially rhomboid as well. Thereby, even when the ends of the claw-like magnetic poles 23 and 24 move at the time of the rotation of the rotor 7, the magnet 30 is not applied with stress and not broken.

The reinforcement 40 is fixed to the claw-like magnetic poles 23 and 24 by an adhesive or the like. Since the reinforcement 40 is made from a metal, the inner faces 23a and 24a of the claw-like magnetic poles 23 and 24 may be welded to the inner portion 40a of the reinforcement 40.

Although the small space S is formed between both side faces 23c or 24c of the claw-like magnetic pole 23 or 24 and the bent portions 40b of the reinforcement 40, an elastic material such as rubber or resin may be placed in this small space S. The elastic material is shaped like a triangular prism, thin plate or rod in conformity with the small space S so that it can be easily inserted into the space. The same effect as described above can be obtained and the elastic material can absorb impact force and suppress the entry of foreign matter.

Embodiment 2

In the above Embodiment 1, the cross section of the reinforcement 40 is substantially M-shaped. In this Embodiment 2, as shown in FIG. 4 and FIG. 5, a reinforcement 41 having a substantially C-shaped cross section is used.

As shown in FIG. 5, the reinforcement 41 consists of a trapezoidal inner portion 41a extended to the inner faces of magnets 31 along the inner face 23a or 24a of the claw-like magnetic pole 23 or 24, bent portions 41b bent outward from both ends of the inner portion 41a and holding the side faces of the magnets 31, and pressing portions 41c projecting from the ends of the bent portions 41b toward the claw-like magnetic pole 23 or 24 and pressing the magnets 31 inward. The pressing portions 41c do not need to cover the entire outer faces of the magnets 31 and extend to intermediate

positions of the outer faces of the magnets 31 to cover more than half the outer faces of the magnets 31 so that they can hold the magnets 31 firmly. There is a gap between the pressing portion 41c and the claw-like magnetic pole 23 or 24 so that part of the outer face of the magnet 31 is exposed.

The magnet 31 is sandwiched between the bent portion 41b of the reinforcement 41 and the side face 23c or 24c of the claw-like magnetic pole 23 or 24 from the inner side and fixed to the claw-like magnetic pole 23 or 24 by holding it on the outer side of the reinforcement 41.

The pressing portion 41c prevents the magnet 31 from falling off from the end of the claw-like magnetic pole 23 or 24 by holding the magnet 31 with the inner portion 41a in a wedge form because the root portion of the magnet 31 is thick.

Since three faces of the magnet 31 are almost surrounded by the reinforcement 41 and the remaining one face of the magnet 31 is in contact with the side face 23c or 24c of the claw-like magnetic pole 23 or 24, the magnet 31 has no large exposed face and has high durability. The magnet 31 can be larger in width than the magnet 30 of Embodiment 1. That is, when attention is paid to the space between the claw-like magnetic poles 23 and 24, the reinforcement 41 does not need to have a portion corresponding to the folded portion 40d of the reinforcement 40 and the thickness in a circumferential direction of the reinforcement 41 is smaller than that of the reinforcement 40. As a result, the magnet 31 becomes larger than the magnet 30 and the output of the car AC generator rises.

Like Embodiment 1, there is a small space S between the side faces 23 or 24 of the claw-like magnetic pole 23 or 24 and the magnets 31 and other portions are fixed by an adhesive or the like. That is, the boundary between the magnet 31 and the bent portion 41b and the pressing portion 41c of the reinforcement 41 is coated with an adhesive and these elements constitute a side magnet body 51.

When the moment of centrifugal force 31E applied to the gravity center 31j of the magnet 31 is taken into consideration, it is the same as in Embodiment 1. That is, the side magnet body 51 displaces in the center direction of the claw-like magnetic pole 23 or 24 with the fulcrum H of the inner portion 41a located at a corner portion between the side face 23c or 24c and the inner face 23a or 24a of the claw-like magnetic pole 23 or 24 as the center of movement.

The difference between Embodiment 1 and Embodiment 2 is that the length of the inner portion 41a covering the inner faces of the magnets 31 of the reinforcement 41 is larger than the length of the inner portion 40a and force for offsetting the spring-back of the reinforcement 41 is larger in Embodiment 2 because the magnets 31 are arranged on the outer side of the reinforcement 41. Thereby, the prevention of the magnets 31 from falling off is promoted and the claw-like magnetic pole 23 or 24 and the magnets 31 are connected to each other more firmly.

As shown in FIG. 6, stopping portions 41n and 41m may be formed by bending the both upper and lower ends of the inner portion 41a of the reinforcement 41. Thereby, the magnets 31 can be prevented from falling off from the end and root sides of the reinforcement 41 without fail. The stopping portions 41n may be formed at both upper and lower ends of the bent portions 41b.

Embodiment 3

In the above Embodiment 1, the small space S is formed between the side faces 23c or 24c of the claw-like magnetic pole 23 or 24 and the bent portions 40b of the reinforcement

40. In this Embodiment 3, as shown in FIGS. 7(a) and 7(b), the magnet 30 is bonded to the pressing portion 40c and the folded portion 40d. The pressing portion 40c, the folded portion 40d and the magnet 30 constitute a side magnet body 50. A small space U is formed between adjacent side magnet bodies 50 and a small space T is formed between the bent portion 40b of the reinforcement 40 and the side face of the magnet 30.

In this case, the center of the movement of the side magnet body 50 differs from those of other embodiments and the side magnet body 50 is supported at one side with the outer end of the bent portion 40b as a fulcrum J. The side magnet body 50 is displaced in a direction opposite to that of Embodiment 1 by the moment of centrifugal force applied to the gravity center of the magnet 30. That is, the side magnet body 50 moves to the adjacent side magnet body 50 in a direction that the folded portions 40d of the adjacent reinforcements 40 are brought close to each other, that is, toward the center in a circumferential direction of the claw-like magnetic pole 23 or 24 to reduce the small space U.

The above small space S may not be formed in this case. When the space is formed, the side face 23c or 24c of the claw-like magnetic pole 23 or 24 and the bent portion 40b of the reinforcement 40 may be bonded together by an adhesive, or an elastic material such as a resin may be placed in the space S and the space S may be smaller than the small space T.

As shown in FIG. 7(b), since the inner side of the side magnet body 50 is displaced in a circumferential direction that the small space U is reduced at the time of the rotation of the rotor 7, the adjacent side magnet body 50 is also displaced in a direction that the small space U is reduced. Then, the folded portions 40d of the reinforcements 40 are contacted to each other and the adjacent side magnet bodies 50 are supported by each other. Thus, unrequired displacement is suppressed, thereby making it possible to improve resistance to centrifugal force at the time of high-speed rotation. Since the reinforcements 40 are contacted to each other, the magnets 30 are not affected. Also, the bent portions 40b of the reinforcements 40 on the claw-like magnetic pole 23 and 24 sides from the fulcrum J as the center of movement are not affected.

Embodiment 4

In the above Embodiment 2, the pressing portion 41c of the reinforcement 41 extends to an intermediate position of the outer face of the magnet 31. In this Embodiment 4, as shown in FIG. 8 and FIGS. 9(a) and 9(b), thin contacting portions 41t and 41t extend to part of the outer face 23b or 24b of the claw-like magnetic pole 23 or 24 from both upper and lower ends of the pressing portion 41c. FIGS. 9(a) and 9(b) are sectional views cut on line B—B and A—A of FIG. 8, respectively.

The contacting portions 41t extend to intermediate positions of chamfered portions 23m or 24m formed at both ends in a circumferential direction of the outer face 23b or 24b of the claw-like magnetic pole 23 or 24 to prevent the reinforcement 41 from falling off from the claw-like magnetic pole 23 or 24 in an inward direction.

This does not require the additional step of processing the claw-like magnetic poles 23 and 24. However, when they are processed for a design reason, they may be processed to a thickness corresponding to the thickness of the contacting portion 41t and its influence upon a magnetic circuit can be ignored. Since part of the contacting portion 41t projects from both ends in an axial direction of the pressing portion

41c of the reinforcement 41, the exposed area of the magnet 31 is secured and coolability is not reduced.

According to this constitution, when the reinforcement 41 and the magnets 31 are to be attached to the claw-like magnetic pole 23 or 24 by an adhesive, they do not need to be held with a jig, thereby making possible a great cost reduction. Also, even when the deterioration of the adhesive with the passage of time is taken into consideration, as the contacting portion 41t and the inner portion 41a of the reinforcement 41 continue to hold the claw-like magnetic pole 23 or 24 and do not lose holding power, a high-reliability and high-quality product can be obtained.

To form the contacting portions in the reinforcement 40, parts of upper and lower ends of the pressing portion 40c may be folded toward the outer face 23b or 24b of the claw-like magnetic pole 23 or 24, or a plate-like contacting piece may be bonded to the pressing portion 40c or 41c.

Embodiment 5

In the above Embodiment 4, the chamfered portions 23m and 24m of the claw-like magnetic poles 23 and 24 are not processed. In this Embodiment 5, as shown in FIG. 10 and FIGS. 11(a) and 11(b), stepped portions 23h and 24h are formed by slightly depressing portions corresponding to the contacting portions 41t and 41t of the chamfered portions 23m and 24m, respectively. The stepped portions 23h and 24h limit the movements in an axial direction of the contacting portions 41t and prevent the reinforcements 41 from falling off from the ends of claw-like magnetic poles 23 and 24. FIGS. 11(a) and 11(b) are sectional views cut on line C—C and A—A of FIG. 10, respectively.

The stepped portions 23h and 24h are formed such that the outer faces 23b and 24b of the claw-like magnetic poles 23 and 24 become almost flush with the contacting portions 41t and 41t when the reinforcements 41 are attached to the claw-like magnetic poles 23 and 24. When the contacting portions 41t and 41t are fitted in the stepped portions 23h and 24h, the reinforcements 41, that is, the magnets 31 are connected to the claw-like magnetic poles 23 and 24 firmly. Therefore, the entire outer surface formed after assembly is a smoothly curved surface which reduces air resistance and does not worsen rotation resistance.

The stepped portions 23h and 24h can be formed by slightly changing the shape of part of each of the chamfered portions 23m and 24m of the claw-like magnetic poles 23 and 24 and do not require separate members to be added. The stepped portions 23h and 24h may be formed with a mold for forming the pole core bodies 21 and 22 or may be formed by processing the chamfered portions 23m and 24m. The stepped portions 23h and 24h can be formed simply by slightly depressing, thereby exerting no magnetic influence upon the claw-like magnetic poles 23 and 24.

As a result, an adhesive for fixing the reinforcement 41 and the magnets 31 to the claw-like magnetic pole 23 or 24 is not necessary, thereby further reducing costs and facilitating production.

Embodiment 6

In the above Embodiment 2, the reinforcements 41 are fixed to the claw-like magnetic poles 23 and 24 by an adhesive alone. In this Embodiment 6, as shown in FIGS. 12(a), 12(b) and 12(c), a ring-form pressing member 60 for pressing the reinforcements 41 against the claw-like magnetic poles 23 and 24 from the inner side is used. This prevents the reinforcements 41 from falling off from the

inner sides or end sides of the claw-like magnetic poles 23 and 24. Compared with Embodiments 4 and 5, the reinforcements 41 are attached to the claw-like magnetic poles 23 and 24 more firmly.

After the reinforcements 41 holding the magnets 31 are located at predetermined positions of the claw-like magnetic poles 23 and 24 as shown in FIG. 12(a), the pressing member 60 having such a diameter that it contacts the center portions of the inner portions 41a of the reinforcements 41 is set as shown in FIGS. 12(b) and 12(c). This pressing member 60 has a peripheral surface which is inclined in conformity with the inclination in an axial direction of the inner portion 41a of each of the reinforcements 41 and has high adhesion with a large adhesion area.

Thereby, the pressing member 60 can hold the reinforcements 41 firmly while the reinforcements 41 are attached to the claw-like magnetic poles 23 and 24, and the AC generator can be carried without a trouble after assembly. A plurality of the reinforcements 41 can be fixed to the claw-like magnetic poles 23 and 24 at the same time and the structure of the reinforcement 41 can be made simple. The pressing member 60 are made from a metal or plastic and may have a rectangular cross section.

When an adhesive is coated to the claw-like magnetic pole 23 or 24 and the reinforcement 41, adhesion surfaces are brought close to each other, thereby making it unnecessary to hold the reinforcements 41 and the claw-like magnetic poles 23 and 24 excessively and securing sufficient adhesion strength. When the plurality of reinforcements 41, the magnets 31 and the pressing member 60 are held by a jig at the time of assembly and connected to the claw-like magnetic poles 23 and 24, fixing by the adhesive is not necessary.

The pressing member 60 may be used for the reinforcements 40. In this case, the inner portions 40a of the reinforcements 40 are pressed by the pressing member 60.

Embodiment 7

In the above Embodiment 6, the peripheral surface of the pressing member 60 contacts the inner portions 40a and 41a of the reinforcements 40 and 41. In this Embodiment 7, as shown in FIG. 13 and FIG. 14, a ring-form pressing member 70 has a cylindrical peripheral surface 70b conformed to the peripheral surface of the rotor 7 and grooves 70m in which the claw-like magnetic poles 23 and 24 held in the reinforcements 40 are fitted are formed in the peripheral surface 70b. As shown in FIG. 14, when the rotor 7 is assembled, the peripheral surface of the rotor 7 forms an almost completely cylindrical curved surface together with the outer faces 23b and 24b of the claw-like magnetic poles 23 and 24.

As shown in FIG. 13, there is a space between the inner wall of the pressing member 70 and the rotor coil 13 and cooling air 70F passes through the space to cool the rotor 7.

Since the reinforcements 40 are thereby pressed from the inner side to the outer side by the pressing member 70 having a large width in an axial direction, they can be connected to the claw-like magnetic poles 23 and 24 more firmly than in Embodiment 6. Further, even when the rotor 7 has a plurality of magnets 30, it has the effect of preventing wind sound from getting worse by rotation because it has a cylindrical curved peripheral surface 70b. The pressing member 70 is wide enough to cover the ends of the claw-like magnetic poles 23 and 24 but may be wide enough to extend to the end surfaces of the base portions 21k and 22k of the pole core bodies 21 and 22.

Embodiment 8

In this Embodiment 8, as shown in FIGS. 15(a) and 15(b), the inclination angles of the side faces 23c and 24c of the

claw-like magnetic poles 23 and 24 are set such that the outer faces 23b and 24b of the claw-like magnetic poles 23 and 24 become wider than the inner faces 23a and 24a. The reinforcements 40 and 41 are formed in conformity with the side faces 23c and 24c which are inclined more.

Thereby, the ends on the inner sides of the magnets 30 and 31 are hardly seen from a circumferential direction and the magnets 30 and 31 are arranged as if they were hidden on the inner face 23a and 24a sides of the claw-like magnetic poles 23 and 24.

In this case, centrifugal force 30E or 31E applied to the magnet 30 or 31 is divided into two segments. That is, resistance 30K or 31K applied to the side face 23c or 24c in a vertical direction increases and dispersion force applied to the side face 23c or 24c in a horizontal direction decreases. Therefore, the centrifugal force resistance of the side magnet body 50 or 51 is improved.

Embodiment 9

In this Embodiment 9, as shown in FIG. 16, the root portion 30n or 31n of the magnet 30 or 31 is made thicker than the end portion 30s or 31s when seen from the cross section in a circumferential direction of the claw-like magnetic pole 23 or 24. In the figure, the reinforcements 40 and 41 are omitted and the shapes of the magnets 30 and 31 are shown when seen from the cross section in a circumferential direction of the claw-like magnetic pole 23 or 24.

That is, the gravity center of the magnet 30 or 31 is located closer to the root side rather than the end side of the claw-like magnetic pole 23 or 24, that is, to the base portion 21k or 22k of the pole core body 21 or 22. Thereby, the displacement of the end portion of the claw-like magnetic pole 23 or 24 which is moved by magnetic attraction force or centrifugal force generated by the rotation of the rotor 7 can be reduced. That is, force influencing the magnet 30 or 31 can be reduced.

As having been described above, according to the first aspect of the present invention, the rotor structure comprises a rotor coil for generating a magnetic flux, a pole core which covers the rotor coil and consists of a first pole core body and a second pole core body, each having a plurality of claw-like magnetic poles which are mated with each other, magnets provided on both sides of each claw-like magnetic pole to suppress the leakage of a magnetic flux between the side faces of adjacent claw-like magnetic poles, and reinforcements for holding the magnets in such a manner that the magnets are inclined so that the interval between the magnets becomes larger on the outer side than on the inner side. Therefore, the magnets can be fixed to each claw-like magnetic pole without fail while they are surrounded by the reinforcement, the strength of a side magnet body composed of the magnet and portions holding the magnet of the reinforcement can be enhanced without taking some measure for the magnets, and the centrifugal force resistance thereof is high.

According to the second aspect of the present invention, the reinforcement consists of an inner portion conformed to the inner face of the claw-like magnetic pole, bent portions bent from both ends of the inner portion toward the side faces of the claw-like magnetic pole, pressing portions, bent from the bent portions, for pressing the outer faces of the magnets, and folded portions folded from the pressing portions toward the side faces of the magnets, and the magnets are held on the inner side of the reinforcement. Therefore, as the reinforcement is easily manufactured at a low cost, has high strength and is formed continuous on the

inner face and the side faces of the claw-like magnetic pole, it can receive centrifugal force and moving force applied to the claw-like magnetic pole with the entire surface from the inner side and can reduce force affecting the magnets.

According to the third aspect of the present invention, the reinforcement consists of an inner portion conformed to the inner face of the claw-like magnetic pole and the inner faces of the magnets, bent portions bent from both ends of the inner portion toward the side faces of the magnets, and pressing portions, projecting from the bent portions toward the claw-like magnetic pole, for pressing the outer faces of the magnets, and the magnets are held on the outer side of the reinforcement. Therefore, as the reinforcement can be easily manufactured at a low cost and is formed continuous on the inner face of the claw-like magnetic pole and the inner faces of the magnets, it can receive centrifugal force and moving force applied to the claw-like magnetic pole with the entire surface from the inner side and can reduce force affecting the magnets.

According to the fourth aspect of the present invention, since the magnet and portions holding the magnet of the reinforcement constitute a side magnet body, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, the side magnet body moves toward the claw-like magnetic pole to reduce the space when centrifugal force is applied to the magnet, and the reinforcement is deformed by this moving force to absorb the centrifugal force. Therefore, even when centrifugal force is generated by the rotation of the rotor, the side magnet body moves and displaces toward the center direction of the claw-like magnetic pole so that it holds the claw-like magnetic pole, whereby the holding power of the reinforcement is strengthened and the centrifugal force resistance thereof is high.

According to the fifth aspect of the present invention, the center of the movement of the side magnet body is located on the claw-like magnetic pole side of the line connecting the center of the rotation axis of the rotor and the gravity center of the magnet, and the movement of the side magnet body is stopped when it contacts the side face of the claw-like magnetic pole. Therefore, even if centrifugal force increases, the side magnet body is firmly fixed, further displacement can be suppressed, centrifugal force is not applied to the magnet, and the centrifugal force resistance of the side magnet body is high.

According to the sixth aspect of the present invention, the magnet is held by the pressing portion and the folded portion and constitutes a side magnet body together with the pressing portion and the folded portion, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, a space is formed between adjacent side magnet bodies, the side magnet body moves toward the adjacent side magnetic body to reduce the space between the adjacent side magnet bodies when centrifugal force is applied to the magnet, the reinforcement is deformed by this moving force to absorb the centrifugal force, and the movement of the side magnet body is stopped when the adjacent folded portions contact each other. Therefore, even when centrifugal force increases, the side magnet body is firmly fixed, further displacement can be suppressed, centrifugal force is not applied to the magnet, and the centrifugal force resistance of the side magnet body is high.

According to the seventh aspect of the present invention, the space between the side magnet body and the side face of the claw-like magnetic pole is set such that the deformed reinforcement can restore its original shape when centrifugal

force is not applied to the magnet after the movement of the side magnet body is stopped and the deformation amount of the reinforcement becomes maximum. When centrifugal force is applied again, the side magnet body can move and the reinforcement can move repeatedly without being broken.

According to the eighth aspect of the present invention, the space between the side magnet body and the side face of the claw-like magnetic pole is set such that stress applied to the reinforcement falls below at least an allowable level when the movement of the side magnet body is stopped and the deformation amount of the reinforcement becomes maximum. Even when the side magnet body moves and displaces maximum, the deformation amount of the reinforcement falls below the allowable level and the reinforcement is not broken by excessive stress.

According to the ninth aspect of the present invention, since an elastic material is placed in the space between the side magnet body and the side face of the claw-like magnetic pole, foreign matter is not contained in the space or impact force to the claw-like magnetic pole can be alleviated at the time of the displacement of the side magnet body.

According to the tenth aspect of the present invention, since the rotor structure has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in an inward direction, the reinforcement is connected to the claw-like magnetic pole more firmly, the magnet is not scattered and not damaged, and the reinforcement does not fall off in an inward direction even when the pole core body fitted with the reinforcements is placed horizontally in an axial direction. Therefore, the rotor structure has excellent work efficiency that it can be freely carried and set.

According to the eleventh aspect of the present invention, since the rotor structure has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in an outward direction, the reinforcement is connected to the claw-like magnetic pole more firmly, the magnet is not scattered and not damaged, the reinforcement does not fall off from the claw-like magnetic pole in an axial direction, and the pole core bodies fitted with the reinforcements can be easily mated with each other with the rotor coil contained therein.

According to the twelfth aspect of the present invention, since the rotor structure has a stopping structure for preventing the reinforcement from falling off from the claw-like magnetic pole in inward and outward directions, the movement of the reinforcement in an inward direction and axial direction with respect to the claw-like magnetic pole can be limited with a simple structure without fail and the holding function of the structure is high.

According to the thirteenth aspect of the present invention, since the above stopping structure is contacting portions which project from the reinforcement and contact the outer face of the claw-like magnetic pole, they have the effect of holding the chamfered portions of the claw-like magnetic pole and preventing the reinforcement from falling off from the claw-like magnetic pole in an inward direction with a simple structure.

According to the fourteenth aspect of the present invention, since a pressing member for pressing the reinforcements against the claw-like magnetic poles from the inner side is used as the stopping structure, the movement of the reinforcements in an inward direction, axially inward direction and axial direction with respect to the claw-like magnetic poles is limited, and pressing force can be applied

to the reinforcements so that the reinforcements are pressed against the claw-like magnetic poles from the inner side.

According to the fifteenth aspect of the present invention, the above pressing member has a cylindrical peripheral surface, grooves in which the claw-like magnetic poles held in the reinforcements are fitted in are formed in the peripheral surface, and the outer faces of the claw-like magnetic poles and the peripheral surface of the pressing member form the cylindrical curved peripheral surface of the rotor. Therefore, the movement of the reinforcements in an inward direction, axially inward direction and axial direction with respect to the claw-like magnetic poles is limited with more certainty, and the entire peripheral surface of the rotor becomes a smoothly curved surface, thereby reducing wind sound generated at the time of the rotation of the rotor.

According to the sixteenth aspect of the present invention, since the side faces of the claw-like magnetic pole are inclined such that the interval between them becomes larger on the outer side than on the inner side, resistance applied to the side faces of the claw-like magnetic pole vertically increases and centrifugal force applied to the magnet alone decreases, thereby increasing the centrifugal force resistance of the side magnet body.

According to the seventeenth aspect of the present invention, since the gravity center of the magnet is located close to the root side of the claw-like magnetic pole, even when the end of the claw-like magnetic pole moves at the time of the rotation of the rotor, the amount of this movement can be reduced.

According to the eighteenth aspect of the present invention, since the reinforcement is made from a metal, it has a high degree of machining freedom and can be manufactured at a low cost.

According to the nineteenth aspect of the present invention, since the reinforcement is welded to the claw-like magnetic pole, it can be firmly connected to the claw-like magnetic pole.

According to the twentieth aspect of the present invention, since the reinforcement has a stopping structure for preventing the magnets from falling off toward the end side or root side of the reinforcement, the magnets can be prevented from falling off from the reinforcement.

What is claimed is:

1. A rotor structure comprising:
a rotor coil for generating a magnetic flux;
a pole core which covers the rotor coil and consists of a first pole core body and a second pole core body, each having a plurality of claw-like magnetic poles which are mated with each other;
magnets provided on both sides of each claw-like magnetic pole to suppress the leakage of a magnetic flux between the side faces of adjacent claw-like magnetic poles; and
reinforcements for holding the magnets in such a manner that the magnets are inclined so that the interval between the magnets becomes larger on the outer side than on the inner side.
2. The rotor structure of claim 1, wherein each of the reinforcements consists of an inner portion conformed to the inner face of the claw-like magnetic pole, bent portions bent from both ends of the inner portion toward the side faces of the claw-like magnetic pole, pressing portions, bent from the bent portions, for pressing the outer faces of the magnets, and folded portions folded from the pressing portions toward the side faces of the magnets, and the magnets are held on the inner side of the reinforcement.

3. The rotor structure of claim 2, wherein the magnet and portions holding the magnet of each of the reinforcements constitute a side magnet body, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, the side magnet body moves toward the claw-like magnetic pole to reduce the space when centrifugal force is applied to the magnet, and each of the reinforcements is deformed by this moving force to absorb the centrifugal force.

4. The rotor structure of claim 3, wherein the center of the movement of the side magnet body is located on the claw-like magnetic pole side of a line connecting the center of the rotation axis of the rotor and the gravity center of the magnet, and the movement of the side magnet body is stopped when it contacts the side face of the claw-like magnetic pole.

5. The rotor structure of claim 3, wherein the space between the side magnet body and the side face of the claw-like magnetic pole is set such that each of the deformed reinforcements can restore its original shape when centrifugal force is not applied to the magnet after the movement of the side magnet body is stopped and the deformation amount of the reinforcement becomes maximum.

6. The rotor structure of claim 3, wherein the space between the side magnet body and the side face of the claw-like magnetic pole is set such that stress applied to each of the reinforcements falls below at least an allowable level when the movement of the side magnet body is stopped and the deformation amount of each of the reinforcements becomes maximum.

7. The rotor structure of claim 3, wherein an elastic material is placed in the space between the side magnet body and the side face of the claw-like magnetic pole.

8. The rotor structure of claim 2, wherein the magnet is held by the pressing portion and the folded portion and constitutes a side magnet body together with the pressing portion and the folded portion, a space is formed between the side magnet body and the side face of the claw-like magnetic pole, a space is formed between adjacent side magnet bodies, the side magnet body moves toward the adjacent side magnetic body to reduce the space between the adjacent side magnet bodies when centrifugal force is applied to the magnet each of, the reinforcements is deformed by this moving force to absorb the centrifugal force, and the movement of the side magnet body is stopped when the adjacent folded portions contact each other.

9. The rotor structure of claim 1 which has a stopping structure for preventing each of the reinforcements from falling off from the claw-like magnetic pole in an inward direction.

10. The rotor structure of claim 9, wherein the stopping structure has contacting portions which project from each of the reinforcements and contact the outer face of the claw-like magnetic pole.

11. The rotor structure of claim 9, wherein a pressing member for pressing the reinforcements against the claw-like magnetic poles from the inner side is used as the stopping structure.

12. The rotor structure of claim 11, wherein the pressing member has a cylindrical peripheral surface, grooves in which the claw-like magnetic poles held in the reinforcements are fitted are formed in the peripheral surface, the outer faces of the claw-like magnetic poles and the peripheral surface of the pressing member form the cylindrical curved peripheral surface of the rotor.

13. The rotor structure of claim 1 which has a stopping structure for preventing each of the reinforcements from falling off from the claw-like magnetic pole in an outward direction.

19

14. The rotor structure of claim 1 which has a stopping structure for preventing each of the reinforcements from falling off from the claw-like magnetic pole in inward and outward directions.

15. The rotor structure of claim 1, wherein the side faces of the claw-like magnetic pole are inclined such that the interval between them becomes larger on the outer side than on the inner side.

16. The rotor structure of claim 1, wherein the center of gravity of the magnet is located close to the root side of the claw-like magnetic pole.

17. The rotor structure of claim 1, wherein each of the reinforcements is made from a metal.

18. The rotor structure of claim 17, wherein each of the reinforcements is welded to the claw-like magnetic pole.

20

19. The rotor structure of claim 1, wherein each of the reinforcements consists of an inner portion conformed to the inner face of the claw-like magnetic pole and the inner faces of the magnets, bent portions bent from both ends of the inner portion toward the side faces of the magnets, and pressing portions, projecting from the bent portions toward the claw-like magnetic pole, for pressing the outer faces of the magnets, and the magnets are held on the outer side of the reinforcement.

20. The rotor structure of claim 1, wherein each of the reinforcements has a stopping structure for preventing the magnets from falling off toward the end side or root side of the reinforcement.

* * * * *